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A P P U N T I

STUDENTE: Chiforeanu Loredana

**MATERIA: Construction of roads,railways and airports - Part 1
- theory slides - Prof. Santagata, Riviera**

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03/10/2017



POLITECNICO DI TORINO
Master Course
in Civil Engineering
2017-18



Construction of Roads, Railways and Airports (01RVMMX)

GENERALITIES
Technical Specifications
Quality control / Quality assurance



General overview

Phases of design and construction of transportation infrastructures

Analysis of feasibility

- Pre-feasibility study
- Feasibility study

Design

- Preliminary design
- Final design
- Executive design

Construction

- Award of contract
- Execution of works
- Measurements and accounting

Final acceptance

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Specifications

Technical specifications

- Characterization and qualification of component materials → it's made by performing tests.
- Construction and placement of materials → production and placement of materials, which can be very detailed.
- Control during construction and on completed works (QC/QA) *Quality control*
Quality Assurance

Reference to relevant standards.

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Specifications

Technical specifications

- PRESCRIPTIVE
- PERFORMANCE-BASED

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Specifications

Technical specifications

➤ PRESCRIPTIVE vs PERFORMANCE-BASED

Performance-based specifications have the **advantage/disadvantage** of reducing the work of the Engineer (no need of continuous testing) and in giving the Contractor freedom in defining the most profitable working strategies.

Performance evaluation eliminates the risk of litigations during construction due to the different interpretation of prescriptive Specifications.

Best option: "hybrid" approach.

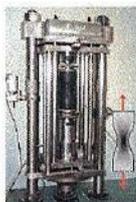
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Specifications

Technical specifications

➤ PRESCRIPTIVE vs PERFORMANCE-BASED

Performance-based specifications require the use of parameters which derive from advanced investigation techniques (e.g. simulative full-scale testing, mechanistically-based laboratory tests).



Mechanistically-based laboratory tests



Full-scale field testing (FWD, structural)



Full-scale field testing (SCRIM, functional)

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Quality Control (QC) and Quality Assurance (QA)

Variability of characteristics of materials and works

Total variability is the sum of several components

- Sampling
- Experimental tests
- Materials
- Construction (production and placement)

Varianza $S^2 = \sigma^2 = (\text{std deviation})^2$

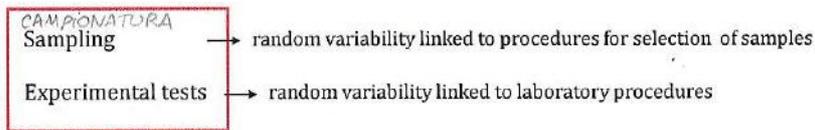
$$S^2_{QC/AC} = S^2_c + S^2_l + S^2_{m/c}$$

Variability = sampling + laboratory tests + material/construction

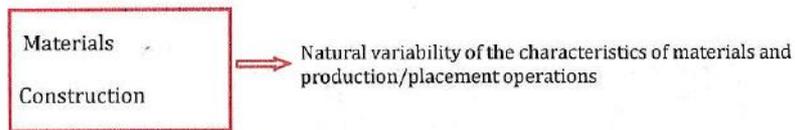
$Var(X+Y) = Var(X) + Var(Y) \rightarrow$

Quality Control (QC) and Quality Assurance (QA)

Variability of characteristics of materials and works



- Can cause more than 50% of total variability
- It is fundamental that operators tightly respect procedures

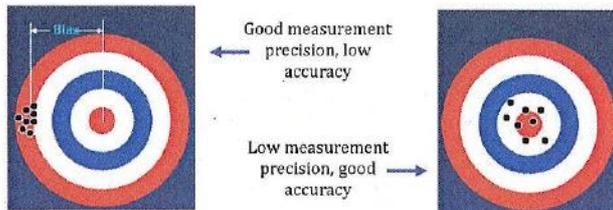


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Quality Control (QC) and Quality Assurance (QA)

Terminology

- Precision = low variability of measurements repeated in control conditions → but they can be far away from the true value.
- Accuracy = conformity of result with respect to true value → you're close to the true value.



All tests have an accuracy and precision assessment, that have been confirmed by many repeated test. Check for calibration and verification, also.

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Quality Control (QC) and Quality Assurance (QA)

Statistical parameters

- Average
- Median value
- Variation range
- Variance

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Quality Control (QC) and Quality Assurance (QA)

Coefficient of variation [Δ] It's dimensionless: serve per comparare cose diverse e per ogni cosa avere il suo (CV) che posso comparare.

$$CV = \frac{\sigma}{\bar{x}} \cdot 100$$

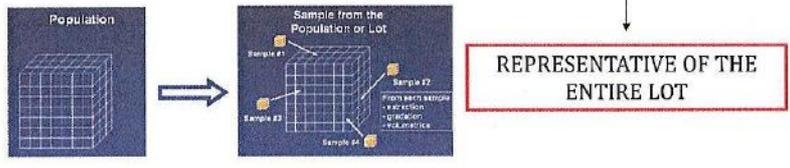
- < 2% = very low variability
- 2 - 5% = low variability
- 5 - 10% = moderate variability
- 10 - 20% = high variability
- > 20% = very high variability

POPULATION ≡ LOT

Quality Control (QC) and Quality Assurance (QA)

Sampling criteria

Determination of a given characteristic referred to a quantity of product (lot) should be performed on a limited number of samples



SAMPLING PROGRAM

- Test frequency
- Location of samples
- Size of samples

Quality Control (QC) and Quality Assurance (QA)

Generation of random positions

Longitudinal (X)

Transverse (Y)

| Sub 1 | Sub 2 | Sub3 | Sub 4 | 43 | X |
|-------|-------|------|-------|----|---|
| 74 | 60 | 01 | 27 | 43 | X |
| 29 | 21 | 78 | 01 | 43 | Y |
| 28 | 37 | 00 | 49 | 97 | |
| 73 | 08 | 87 | 32 | 97 | |
| 72 | 14 | 09 | 70 | 41 | |

A local system of cartesian coordinates is define for each sub-lot

A random sequence of numbers is generated

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Quality Control (QC) and Quality Assurance (QA)

Generation of random positions

Generated numbers are multiplied by the transversal dimension of the sub-lot

Exeample → Rectangular shape 100 m x 12 m

Sub-lot 1

- Coordinate X = 0,74 x 100 = 74 m
- Coordinate Y = 0,29 x 12 = 3,5 m

Sub-lot 2

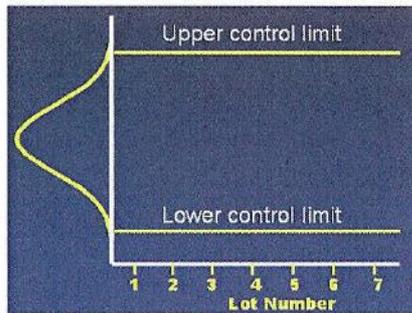
- Coordinate X = 0,60 x 100 = 60 m
- Coordinate Y = 0,21 x 12 = 2,5 m
- ... etc.

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Quality Control (QC) and Quality Assurance (QA)

CONTROL CHARTS - Usage criteria

It can be considered as a sequence of normal distribution curves (vertical axis) as a function of tested samples (lots)



It can be assumed that the process is "under control" when the values are contained within the upper and lower limits



Average $\pm 3\sigma$

In the axis, I can choose what to put (time, distance)

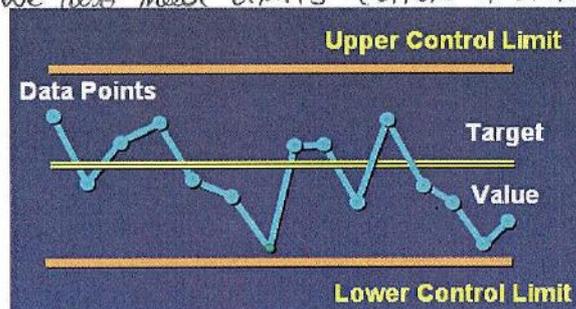
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Quality Control (QC) and Quality Assurance (QA)

CONTROL CHARTS - Usage criteria

A fundamental characteristic of this approach is the possibility of distinguishing random variability from systemic variability due to a specific cause

We also need LIMITS (UPPER AND/OR LOWER)



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Quality Control (QC) and Quality Assurance (QA)

CONTROL CHARTS - Interpretation

There is a problem (the system is not under control any more) when:

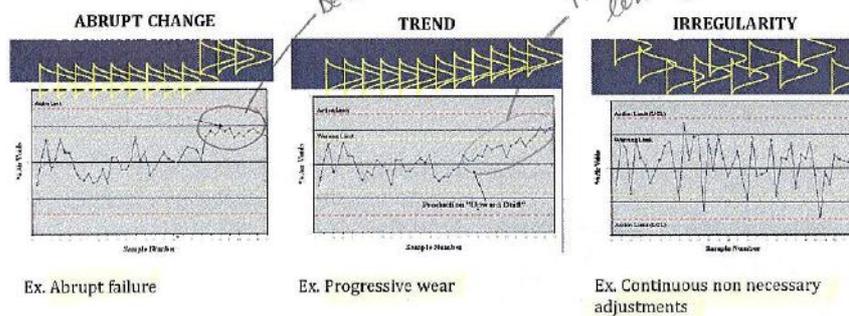
- \bar{X} varies, R constant
- \bar{X} constant, R varies
- \bar{X} e R vary

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Quality Control (QC) and Quality Assurance (QA)

CONTROL CHARTS - Interpretation

Example: Variation of average



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Quality Control (QC) and Quality Assurance (QA)

QUALITY INDEXES

$$Q(U) = \frac{USL - \bar{X}}{\sigma}$$

$$Q(L) = \frac{\bar{X} - LSL}{\sigma}$$

lower specification limit.

USA table

VARIABILITY - UNKNOWN PROCEDURE
STANDARD-DEVIATION METHOD

PWL

| Quality Index (Q _U or Q _L) | Percent Within Limits for Selected Sample Sizes | | | | | | | |
|---|---|--------|--------|--------|--------|--------|--------|--------|
| | N = 3 | N = 4 | N = 5 | N = 6 | N = 7 | N = 8 | N = 9 | N = 10 |
| 1.50 | 100.00 | 100.00 | 96.20 | 95.19 | 94.72 | 94.44 | 94.26 | 94.13 |
| 1.55 | 100.00 | 100.00 | 97.13 | 96.00 | 95.48 | 95.17 | 94.97 | 94.82 |
| 1.60 | 100.00 | 100.00 | 97.97 | 96.75 | 96.17 | 95.84 | 95.62 | 95.48 |
| 1.65 | 100.00 | 100.00 | 98.72 | 97.42 | 96.81 | 96.45 | 96.22 | 96.05 |
| 1.70 | 100.00 | 100.00 | 99.34 | 98.02 | 97.38 | 97.01 | 96.76 | 96.59 |
| 1.75 | 100.00 | 100.00 | 99.81 | 98.55 | 97.89 | 97.51 | 97.25 | 97.07 |
| 1.80 | 100.00 | 100.00 | 100.00 | 98.99 | 98.35 | 97.96 | 97.70 | 97.51 |
| 1.85 | 100.00 | 100.00 | 100.00 | 99.36 | 98.74 | 98.35 | 98.09 | 97.91 |
| 1.90 | 100.00 | 100.00 | 100.00 | 99.66 | 99.07 | 98.67 | 98.44 | 98.25 |
| 1.95 | 100.00 | 100.00 | 100.00 | 99.86 | 99.35 | 98.95 | 98.74 | 98.55 |
| 2.00 | 100.00 | 100.00 | 100.00 | 99.97 | 99.57 | 99.24 | 99.00 | 98.83 |
| 2.05 | 100.00 | 100.00 | 100.00 | 100.00 | 99.74 | 99.45 | 99.23 | 99.05 |
| 2.10 | 100.00 | 100.00 | 100.00 | 100.00 | 99.86 | 99.61 | 99.41 | 99.25 |
| 2.15 | 100.00 | 100.00 | 100.00 | 100.00 | 99.94 | 99.74 | 99.57 | 99.42 |
| 2.20 | 100.00 | 100.00 | 100.00 | 100.00 | 99.99 | 99.84 | 99.69 | 99.56 |
| 2.25 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.91 | 99.79 | 99.68 |
| 2.30 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.96 | 99.86 | 99.77 |
| 2.35 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.98 | 99.92 | 99.84 |
| 2.40 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.95 | 99.89 |
| 2.45 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.98 | 99.93 |
| 2.50 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.99 | 99.96 |
| 2.55 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.98 |
| 2.60 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 99.99 |
| 2.65 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |

Numbers in the body of this table are estimates of percent within limits (PWL) corresponding to specific values of Q, the QUALITY INDEX. For Q values less than zero, subtract the table value from 100.

NOTE: More detailed tables ($\Delta Q = 0.01$) can be developed from more accurate values of PWL.

AASHTO QC/QA Guide Spec. Page 21

Parameters P_U or P_L (AASHTO)

EX: How variability affects the values because of the dispersion.

Quality Control (QC) and Quality Assurance (QA)

ACCEPTANCE - PWL

Same average, different degree of dispersion

$CV_1 = \frac{0,20}{5}$

$CV_2 = \frac{0,4}{5} = 8\%$

→ good
→ not good → lower quality

Same standard deviation, different average value

→ is a little bit out of limits.

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Construction of Roads, Railways and Airports (01RVMMX)

EARTHWORKS - SOIL
 Classification, compaction, bearing capacity



EARTH WORKS
 comprehend the work of filling and cutting the ground.

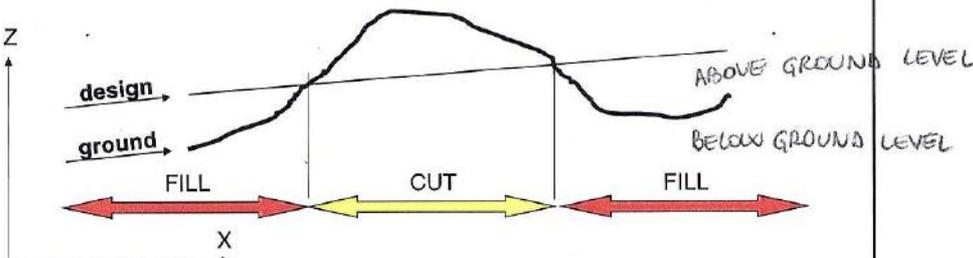
It's important the construction and the economics related to the movements a construction of soils.

soil ← FULLY DRY
 PARTIALLY SATURATED
 FULLY SATURATED

General concepts on earthworks

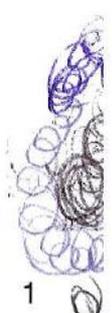
Road prism / *SOLIDO STRADALE*

Cross section delimited by road platform (including marginal elements), original ground and lateral slopes.
 Obtained by means of earthworks with the cutting of trenches and construction of embankments.

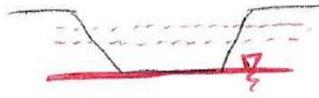


The diagram shows a cross-section with a vertical Z-axis and a horizontal X-axis. A solid line represents the 'design' level, and a dashed line represents the 'ground' level. The area between the design and ground lines is divided into three sections: 'FILL' (indicated by red arrows pointing outwards), 'CUT' (indicated by a yellow arrow pointing inwards), and 'FILL' (indicated by red arrows pointing outwards). The top of the design line is labeled 'ABOVE GROUND LEVEL' and the bottom of the ground line is labeled 'BELOW GROUND LEVEL'. The word 'RILEVATI' is written below the diagram.

*TRINCEA
 MEZZA COSTA
 RILEVATO*

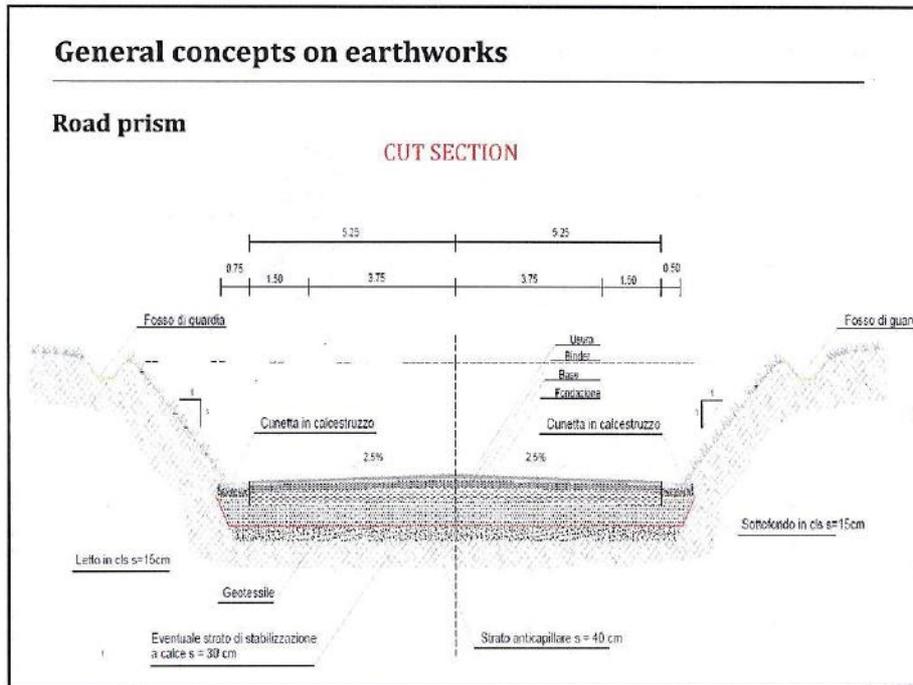


If I have this situation:

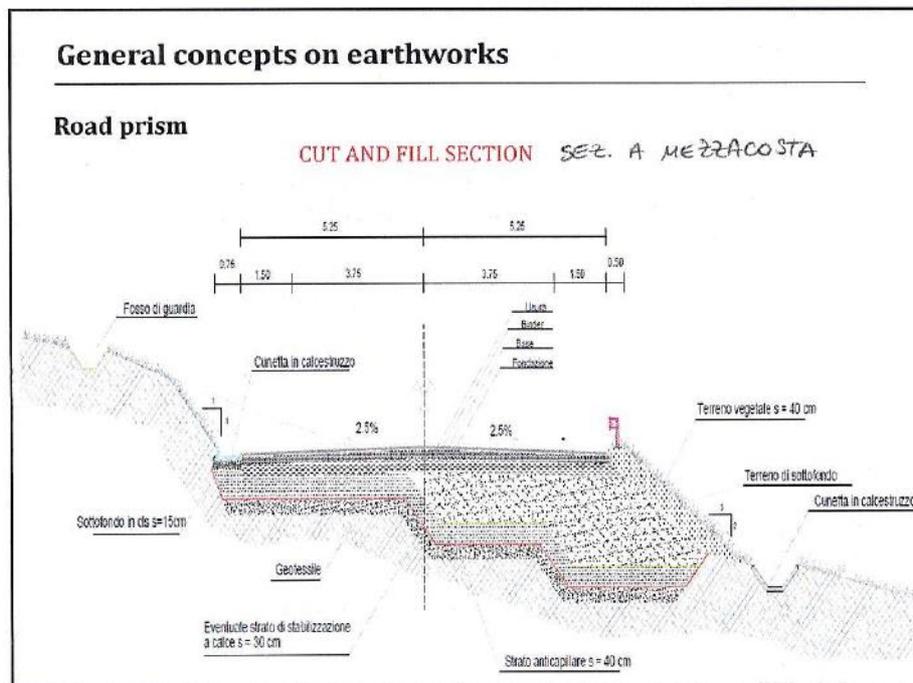
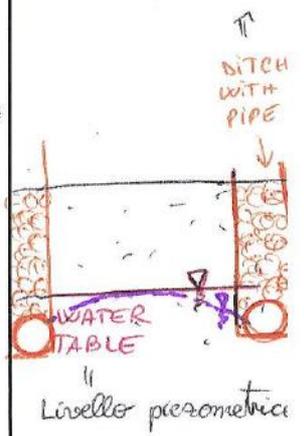


⇒ I need to lower the level of water

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fossi/tras con tub



SOIL RICHIAMI

Soils are formed from several alteration processes:

- physical (decompression)
- chemical (action of O₂, CO₂, acids)
- organic (acids, bacteria)
- mechanical (erosion, impact)

**Three-phase system
SOLID + LIQUID + AIR**

Volumi

Masse

PICNOMETER ⇒ measure volume of grains : the volume of grains is the volume displaced ^{of H₂O}.

SOIL RICHIAMI

Definitions

- Water content *it can change*
 $w[\%] = \frac{W_w}{W_s} \cdot 100 = \frac{W - W_s}{W_s} \cdot 100$
→ STATE VARIABLE
- Grain density *DENSITÀ DEL GRANO*
 $\gamma_s = \frac{W_s}{V_s}$
- Apparent density *DENSITÀ APPARENTE*
 $\gamma = \frac{W}{V} = \frac{W_w + W_s + W_a}{V_s + V_v + V_w}$
- Dry density *DENSITÀ SECCA*
 $\gamma_s = \frac{W_s}{V} = \frac{W_s}{V_s + V_v + V_w}$

Volumi

Masse (Pesi)

- Void index *INDICE DEI VUOTI*
 $e = \frac{V_v + V_w}{V_s}$
- Porosity *POROSITÀ*
 $n = \frac{V_v + V_w}{V}$

w = weight

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RICHIAMI

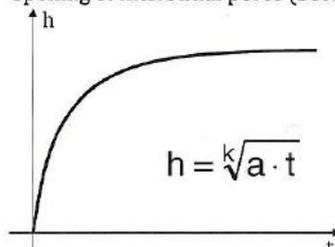
SOIL

Capillarity

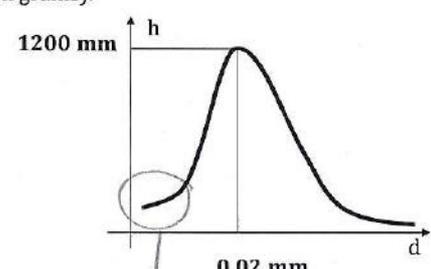
In unsaturated soils capillarity tensions can occur and these may cause the upward motion of water.

The height by which free water can move upwards by capillarity (h) depends upon:

- time;
- opening of interstitial pores (between grains).



$h = \sqrt{k a \cdot t}$



1200 mm

0,02 mm

SILT → capillar reaction.

in the compacted clay there is no capillarity.

RICHIAMI

SOIL

Frost effects

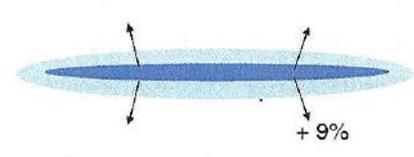
Effect of low temperatures ($T < 0^\circ\text{C}$) in the winter period:

- formation of ice lenses (volume increase);
- expansion;
- spring thaw with volume reduction and loss of bearing capacity.

LENTI DI GHIACCIO

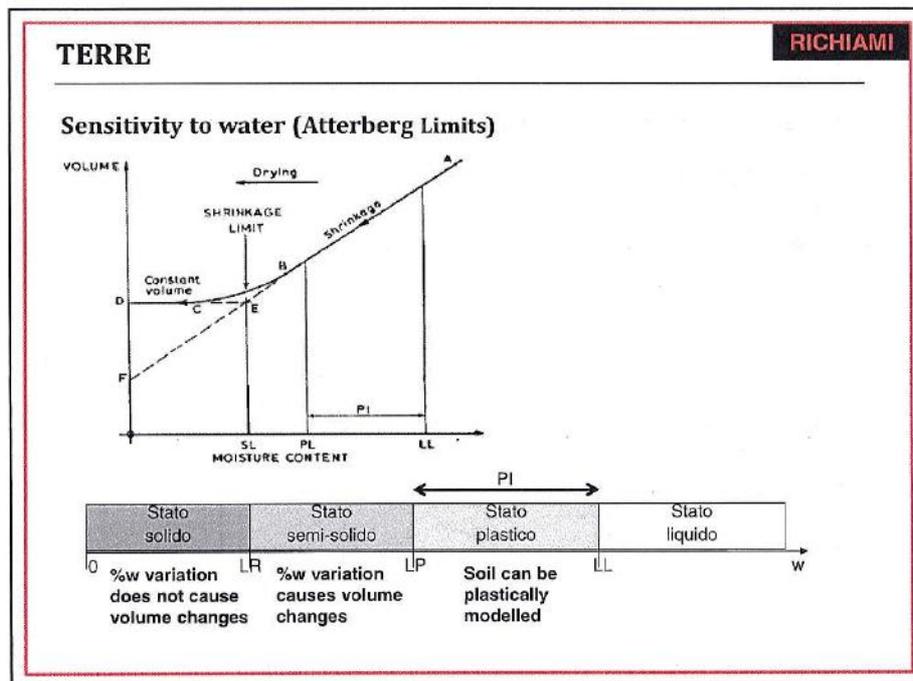
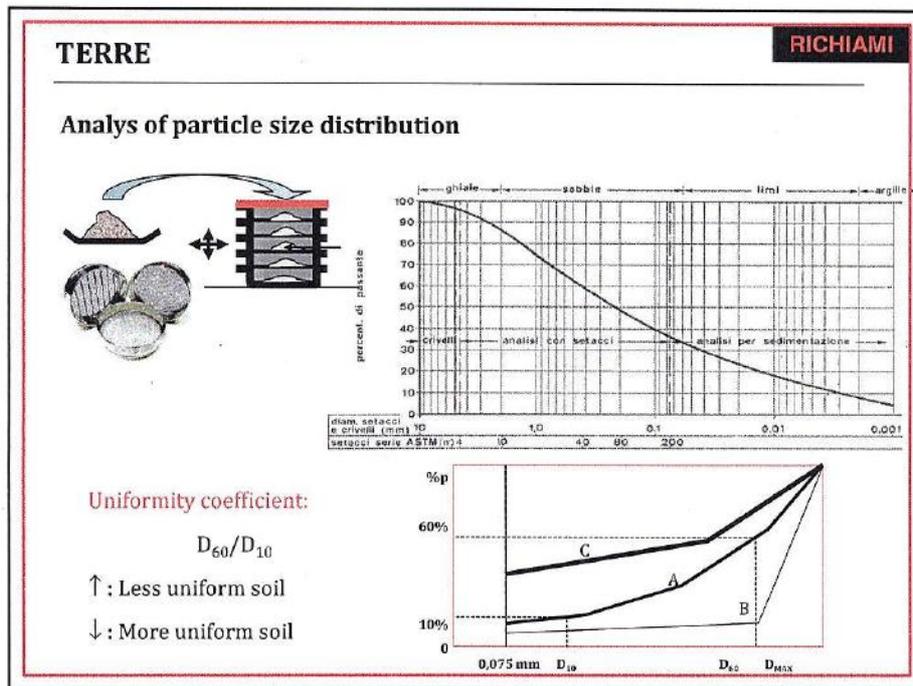
Conditions:

- soil size distribution;
- position of water table;
- climatic conditions (depth of frost penetration).



+ 9%

The crystals of ice tend to attract other water and increase its dimension. In spring ice melts [defrosting] and the structure collapses.



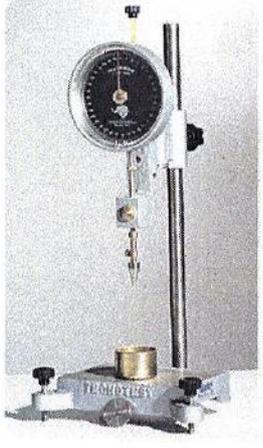
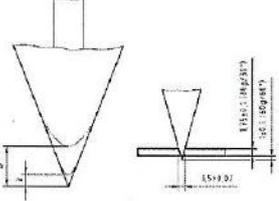
SOIL

Liquid limit - methods of measurement

UNI CEN ISO/TS 17892-12:2005

Tests carried out on material passing at the 0.425 mm sieve

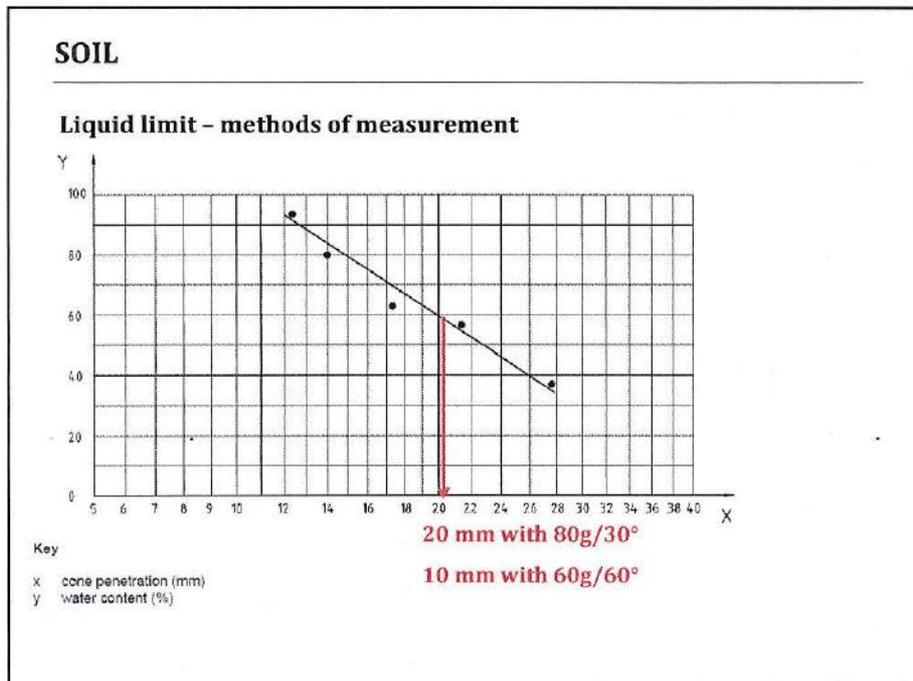
Cone penetrometer

Two geometries:

- 60g/60°
- 80g/30°

NEW METHOD



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TERRE

Classificazione delle terre

È uno strumento di valutazione preventiva delle prestazioni delle terre basato sulle dimensioni e sulla sensibilità all'acqua.

Requisiti:

- significato preciso dei parametri considerati;
- facile e quasi immediata determinazione dei risultati;
- apparecchiature semplici ed utilizzabili anche in cantiere;
- parametri non dipendenti dallo stato del terreno (umido o asciutto), dalle condizioni di sollecitazione e dalle condizioni ambientali.



CONSENTE DI DISCRIMINARE I TERRENI IDONEI ALL'USO PER LE COSTRUZIONI STRADALI DA QUELLI NON IDONEI

TERRE

Classificazione delle terre

Le prove contemplate dal sistema di classificazione sono le seguenti:

1. **analisi granulometrica** ai vagli n.10 (2 mm), n.40 (0,425 mm) e n.200 (0,063 mm);
2. **limite liquido (LL)**;
3. **indice di plasticità (IP)**;
4. **indice di gruppo** (indicatore sintetico) la cui formula è la seguente:

$$IG = (P_{75\mu m} - 35) \cdot [0,2 + 0,005 \cdot (LL - 40)] + 0,01 \cdot (P_{75\mu m} - 15) \cdot (IP - 10)$$

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TERRE

Classificazione delle terre

PRIORITA' D'IMPIEGO (AGGIORNATA)

- **CORPO DEL RILEVATO:** gruppi A1, A3 (se necessario confinate), A2-4, A2-5, A4 (con indice di gruppo pari a 0), A2-6, A2-7 (parte bassa del rilevato, a distanza si almeno 2 m dal piano di posa della sovrastruttura e previa disposizione di uno strato anticapillare);
- **SOTTOFONDO:** gruppi A1, A2-4, A2-5, A3 (con coefficiente di uniformità maggiore di 7);
- **RILEVATI FERROVIARI E SUPERCOMPATTATI:** gruppi A1, A2-4, A2-5, A2-6, A2-7, A3 (in base alla granulometria), A4 per il rilevato, A1, A2-4 e A3 (in base alla granulometria)

TERRE

Classificazione delle terre

Gruppo A₁ - Appartengono a questo gruppo i materiali rocciosi non evolutivi e le terre granulari, generalmente di più o meno grossa pezzatura, pressoché insensibili all'azione dell'acqua e del gelo, che sotto il profilo dei movimenti di terra possono dar luogo ad un ampio spettro di comportamenti, in relazione:

- al contenuto di fino (frazione minore di 0,075 mm);
- all'assortimento granulometrico;
- alla presenza di elementi di grossa pezzatura.

Nel prevederne l'impiego occorre considerare che le ghiaie e le sabbie alluvionali con poco fino (meno del 5%), permeabili e prive di coesione, dopo costipamento risultano tanto più soggette all'erosione dell'acqua meteorica quanto più l'assortimento granulometrico è mal graduato. Per evitare che possano prodursi danni, l'Impresa deve rigorosamente procedere al rivestimento con terra vegetale delle scarpate man mano che cresce l'altezza del rilevato; la semina per l'inerbimento, ugualmente, deve essere effettuata il più rapidamente possibile.

I detriti di falda, le rocce alterate, i depositi morenici ed anche le alluvioni eterogenee con un contenuto di fino compreso tra il 10 ed il 15% danno luogo a strati molto compatti e difficilmente erodibili; richiedono, tuttavia, un attento controllo dell'umidità di costipamento al fine di attingere valori elevati di portanza. I materiali con elementi superiori a D=50mm e, in particolare, quelli provenienti da scavi in roccia (dura e tenace) richiedono cautele e particolari provvedimenti per quel che riguarda la stesa in strati di spessore regolare ed il costipamento.

I provvedimenti da adottarsi consistono nelle seguenti operazioni:

- scarto degli elementi di dimensioni maggiori di D=500 mm;
- correzione granulometrica (per frantumazione e/o aggiunta di pezzature in difetto).

Nella redazione del piano dei movimenti di terra, di norma si riservano le terre del sottogruppo A1-a, specialmente se di granulometria ben assortita, ai manufatti in terra che richiedono più elevate proprietà meccaniche e/o agli strati di sottofondo.

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TERRE

Classificazione delle terre

Sottogruppi A_{2.6} e A_{2.7} Le ghiaie e le sabbie argillose di questi sottogruppi sono, di norma, convenientemente utilizzate per la formazione dei rilevati, specialmente quando presentano un indice di gruppo IG=0. Il loro comportamento, tuttavia, è molto influenzato dalla quantità e dalla natura della frazione argillosa presente. Portanza e caratteristiche meccaniche attingono valori intermedi tra quelle delle ghiaie e delle sabbie che costituiscono l'ossatura litica del materiale e quelle delle argille che costituiscono la frazione fine. Poste in opera, esse presentano da media a bassa permeabilità ed altezza di risalita capillare, ciò che determina elevato rischio di formazione di lenti di ghiaccio per azione del gelo. Per questo motivo, in presenza di falda superficiale e di prolungata durata di condizioni climatiche di bassa temperatura, il loro impiego deve essere evitato nella formazione di strati di sottofondo e limitato agli strati posti al di sotto di 2,00 m dal piano di posa della pavimentazione stradale, previa predisposizione, a quota inferiore, di uno strato anticapillare di spessore non inferiore a 30 cm.

L'energia e l'umidità di costipamento delle terre dei sottogruppi in esame debbono essere costantemente controllate; quando il contenuto d'acqua risulta prossimo o supera il limite di plasticità della frazione fine si rischia, infatti, di provocare instabilità e cadute di portanza per sovracostipamento del materiale. Se lo stato delle terre e le condizioni ambientali non obbligano alla sospensione dei lavori, è opportuno adottare basse energie di costipamento, operando su strati di modesto spessore.

TERRE

Classificazione delle terre

Gruppi A₄, A₅, A₆ e A₇ L'opportunità d'adoperare terre di questi gruppi deve essere valutata secondo le seguenti linee guida:

- disponibilità di terre sostitutive, anche in relazione alle distanze di trasporto ed alle esigenze di carattere ambientale;
 - provvedimenti da adottare per la protezione da venute d'acqua (gravitazionali o di capillarità) nelle opere in terra con esse realizzate;
 - tecniche di miglioramento, quale il trattamento a calce, finalizzate a ricondurre le proprietà fisico-chimiche e meccaniche entro limiti di garanzia delle prestazioni, nel volgere della vita economica dell'opera.
- Per l'impiego dei materiali dei gruppi A₄ ed A₅ occorre considerare che:
- la consistenza di queste terre (-IP<10) cambia sensibilmente per modeste variazioni del contenuto d'acqua;
 - anche per modesti incrementi d'umidità si passa rapidamente da comportamenti tipici di terreni asciutti, difficili da compattare, a quelli di terreni troppo umidi, per i quali risulta talvolta impossibile ottenere il grado di addensamento richiesto;
 - in relazione all'assortimento granulometrico ed all'addensamento, la permeabilità ed il potere di risalita capillare possono variare entro limiti abbastanza ampi; ne risulta un forte potere di imbibizione (portate d'invasamento capillare) e, quindi, un'estrema sensibilità al rigonfiamento ed all'azione del gelo. I rilevati realizzati con questi terreni, pertanto, debbono essere protetti dalle acque interne ed esterne, mediante strati anticapillari, schermi drenanti, tempestivi rinfianchi laterali con inerbimento;
 - la presenza di ciottoli ed elementi di più grossa pezzatura può impedire l'azione dei mezzi di miscelazione e, quindi, renderne impossibile la stabilizzazione a calce.

Le difficoltà di compattazione delle argille dei gruppi A₆ ed A₇, le proprietà meccaniche generalmente modeste degli strati, come pure i provvedimenti di difesa dalle acque da mettere in atto limitano l'impiego di queste terre a rilevati di modesta importanza. Se non sono presenti elementi di grosse dimensioni, le terre dei gruppi A₆ ed A₇ si prestano bene alla stabilizzazione con calce.

09/10/2017

SOILS
REVIEW

Physical and mechanical properties

Soil behaviour depends upon:

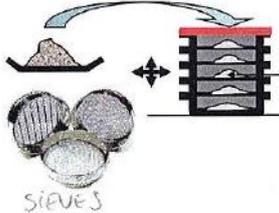
- size distribution of particles;
- presence of water and sensitivity which particles have in interacting with it.

On representative soil sample the following aspects are evaluated:

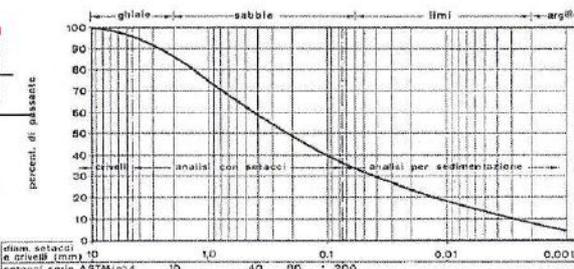
- percentage of size fractions;
- sensitivity to water (of finer fractions).

SOILS
REVIEW

Analysis of particle size distribution *cumulative percent curve*



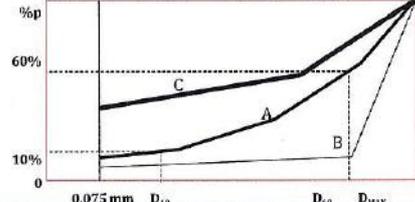
SIEVES



Uniformity coefficient:

$$D_{60}/D_{10}$$

↑ : Less uniform soil
↓ : More uniform soil



size of particles \equiv open of sieves

Uniform soil: problem in compacting the soil

09/10/2017

SOILS → it's sensitive to the experience of the operator

Liquid limit - methods of measurement

Tests carried out on material passing at the 0.425 mm sieve. includes also FINE SAND

LL - Liquid limit (Casagande apparatus)

OLD METHOD

SEMI-LOGARITMIC PLOT

4 TESTS

3 difference between OLD and NEW.

SOILS

Liquid limit - methods of measurement

UNI CEN ISO/TS 17892-12:2005

Tests carried out on material passing at the 0.425 mm sieve

Cone penetrometer

Two geometries:

- 60g/60°
- 80g/30° → corresponds to the application of a load of 80g.

NEW METHOD

final penetration after 5 s.

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The difference between old and new is in preparation of cylinders.

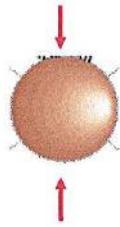
SOILS

Plastic limit - methods of measurement

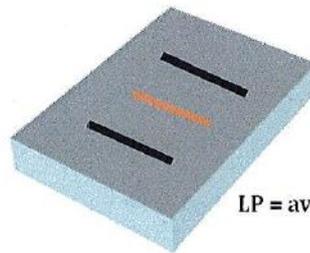
UNI CEN ISO/TS 17892-12:2005

20 g of moist soil

BALL



Two 10 g portions (sub-samples)



LP = average of two repetitions

NEW METHOD

$\frac{2}{4}$ of ball is made in cylinders.

SOILS

Classification of soils

It is a tool for the preliminary evaluation of soil performance based on particle size and sensitivity to water.

Requisites:

- clear meaning of considered parameters;
- easy and quick determination of results;
- simple equipment which can be used in field laboratories;
- parameters which do not depend on soil state (wet or dry), on stress conditions and environmental conditions.

MEASUREMENTS HAS TO BE INTRINSIC



ALLOWS THE DISTINCTION BETWEEN SOILS WHICH CAN BE USED FOR EARTHWORKS AND THOSE WHICH MAY NOT

09/10/2017

SOILS

Classification of soils - HRB system (UNI 11531-1:2014)

PRIORITY OF USE (general)

- Groups A1, A2-4, A2-5, A3;
- Groups A2-6 and A2-7.

For soils belonging to groups A4, A5, A6 and A7 it should be considered whether:

- to use the with proper attention (protection from water);
- to proceed with treatment/improvement (e.g. lime stabilization),
- to exclude their use and proceed with disposal. *EXAMPLE GIVEN*

SOILS

Classification of soils - HRB system (UNI 11531-1:2014)

PRIORITY OF USE (specific)

- **EMBANKMENT:** Groups A1, A3 (confined, if necessary), A2-4, A2-5, A4 (with group index equal to 0), A2-6, A2-7 (lower part of embankment, at least at 2 m from pavement support level, with anti-capillary layer);

- **SUBGRADE:** Groups A1, A2-4, A2-5, A3 (with uniformity coefficient greater than 7);

PREMIUM QUALITY SOILS

- **RAILWAY EMBANKMENTS:** Groups A1, A2-4, A2-5, A2-6, A2-7, A3 (depending upon particle size distribution), A4 for embankment

- **RAILWAY SUBGRADE:** Groups A1, A2-4 e A3 (depending upon particle size distribution)

→ if it increases is good.

→ EXTRA - CHECK OF SAND,

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SOIL COMPACTION

Goals of compaction

- reduce further settlements during service life of infrastructure as a result of static loads (permanent) and of dynamic loads (transient);
- improve mechanical properties of soils (mainly friction angle ϕ), to satisfy construction requirements (sufficient stiffness of each layer, necessary for compaction of layers above) and to ensure stability of construction work in service;
- reduce the influence of water (lower porosity leads to lower permeability and increased resistance to erosion).

SLOPES NOT TO FAIL (collassare),

USE ROLLERS

SOIL COMPACTION

INCREASE DENSITY

Description of phenomenon

Porosity reduction generated by compaction is due to:

- expulsion of air contained in soil volume,
- migration of water (minimal contribution since compaction is a quick phenomenon unlike consolidation: water content does not change dramatically) → BUT YOU CAN'T DRY THE SOIL WITH COMPACTION
- compression of air which cannot be expelled (especially for clayey soils)

FACTORS WHICH INFLUENCE COMPACTION:

1. Soil type (A)
2. Water content (w)
3. Compaction energy (E)
4. Compaction mode
5. Layer thickness and stiffness of support → energy is differently distributed

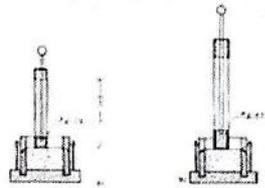
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SOIL COMPACTION *At least 5 test at ≠ water content.*

Proctor test - experimental procedure

UNI EN 13286-2 (2005)

- Type A (AASHTO Standard - T 99)
- Type B (AASHTO Modificata - T 180)



| | Standard | Modificato |
|--|----------|------------|
| numero di strati | 3 | 5 |
| massa del pestello | 2,495 kg | 4,535 kg |
| altezza di caduta | 30,5 cm | 45,7 cm |
| numero di colpi | 25 - 56 | 25 - 56 |
| energia per unità di volume [N/cm ²] | 59 | 269 |

$$E = \frac{P_{\text{maglio}} \cdot h \cdot n_c \cdot n_s}{V_{\text{fustella}}} \quad \text{Compaction energy per unit volume}$$

development of new rollers

SOIL COMPACTION

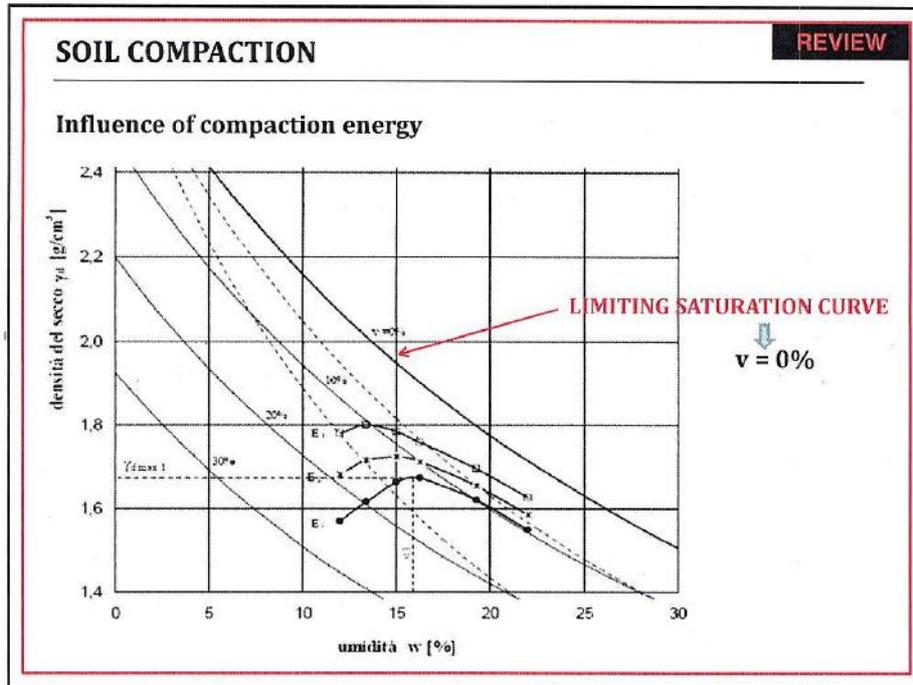
Proctor test - experimental procedure

Amount of soil for 5 determinations:

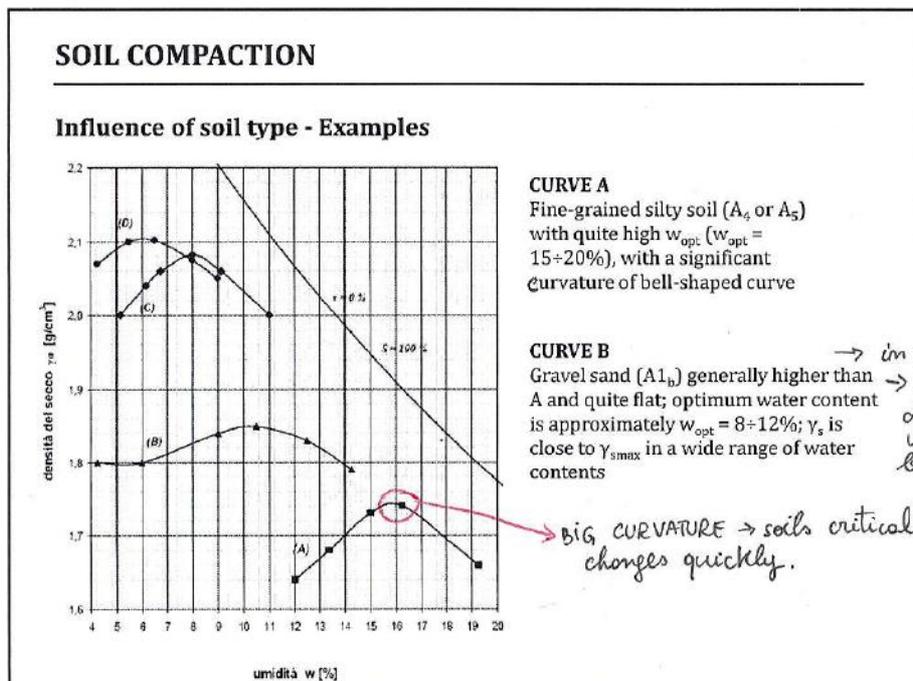
- 15 kg for small mould
- 36 kg for large mould

Procedure:

- drying at 50°C and disgregation;
- sieving at sieve 25 mm (if the retained is higher than 35 % of total mass the test cannot be performed);
- choice of small/large mould (small is the passing at 25 mm is entirely passing at 5 mm - n.4 ASTM);
- formation of single specimens (variable water contents).

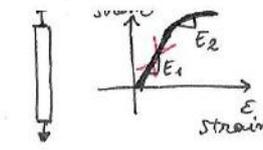


Different curves that refer to ≠ types of soil



Variation stress depends on the velocity of a vehicle, distance from the vehicle,

ex



$E_2 < E_1$

10/10/2017

stress ↑ → stiffness or ↑ E

$E_1 = \text{linear elasticity}$
 $E_2 = \text{non-linear elasticity}$



↑
 Stiffness is important, It's not the same in every point.

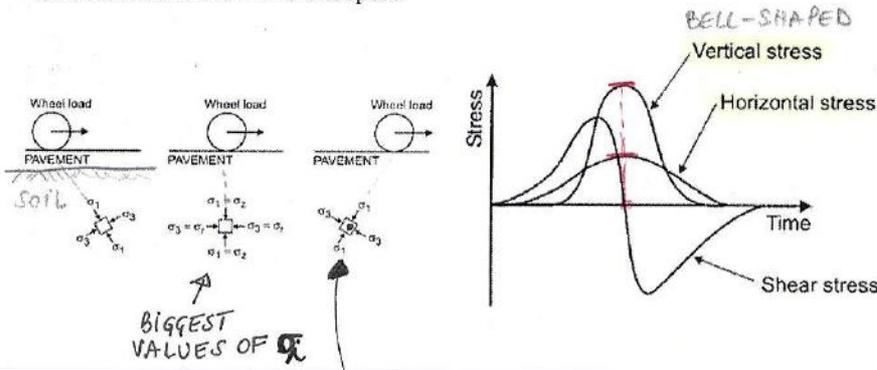
↑
 Deformation (strain) of soils

SOIL MECHANICS

Mechanical behaviour of soils

As a result of moving traffic the following occurs:

- rotation of principal planes (on which principal stresses arise)
- variation of stresses as a function of time
- dependency of elastic response from the state of stress
- variation of stresses with traffic speed



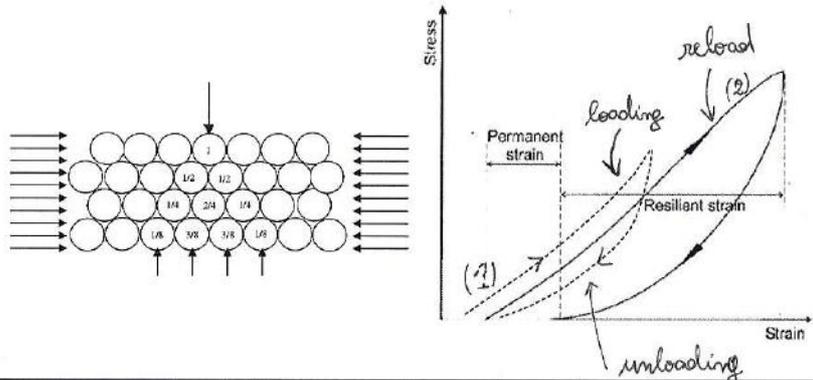
Ⓜ
 Variation of stresses as a function of time.
 ⊕
 Rotation of stresses
 ↓
 PRINCIPAL
 principal stress is POINTING AT THE VEHICLE

cube that represents a point, at a generic deep, on which we have normal and tangential stresses.

SOIL MECHANICS

Mechanical behaviour of soils

- not perfectly elastic
- strain response depends upon lateral confinement
- stiffness depends upon stress state (non-linearity) and stress history



The response can change in time. The stress history affects the future behaviour of the material.

CBR was born to define a value for a thickness of pavement. Then its result is used also for other purposes.

It's a shear and stiffness test, that shows the general behaviour of the material. 10/10/2017

SOPPORTARE

CBR Method (California Bearing Ratio)

Describes the aptitude of the material to bear stress.

TEST

1. Position mould in loading frame
2. Apply surcharge
3. Apply load with a speed of displacement equal to 1,27 mm/min
4. Reading of applied pressure corresponding to displacements of: 0,5, 1, 1,5, 2, 2,5, 3, 4, 5, 7 e 9 mm

$$CBR = \max \left(\begin{array}{l} 100 \frac{P_{2,5mm}}{P_{RIF-2,5mm} (70kg/cm^2)} \\ 100 \frac{P_{5mm}}{P_{RIF-5mm} (105kg/cm^2)} \end{array} \right)$$

↓
EMPIRICAL APPROACH

of the material to bear stress.

DYNAMOMETRIC RING

ring with a hole.

moves upwards with a given speed

Pressure applied increases as the penetration in the sample increases.

→ Focus on the value of pressure corresponding to the given penetrations of 2,5 and 5 mm

We obtain 2 values and take the maximum ← compare the result with the reference value of $P_{2,5} = 70 \frac{kg}{cm^2}$ and $P_5 = 105 \frac{kg}{cm^2}$

CBR Method (California Bearing Ratio)

NEED TO CORRECT

CORRECTED CBR INDEX
Obtained by shifting the origin of pressure-displacement plot

CBR INDEX AFTER SATURATION
Obtained by carrying out the test after 4 days of immersion in water. This is generally done because we need to check in the worse condition

THE CURVE:
- shift the R.S.
- recalculate the pressures.

change of curvature

During immersion the soils can expand → we can measure the expansion putting an instrument.
= reference values also in technical specifications.

10/10/2017

RESILIENT MODULUS

Repeated loading triaxial tests (AASHTO T294) $H = 2\phi$

The test simulated the stress-strain state which results from vehicles

RATIONAL APPROACH

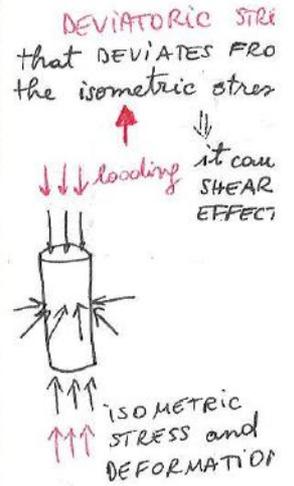
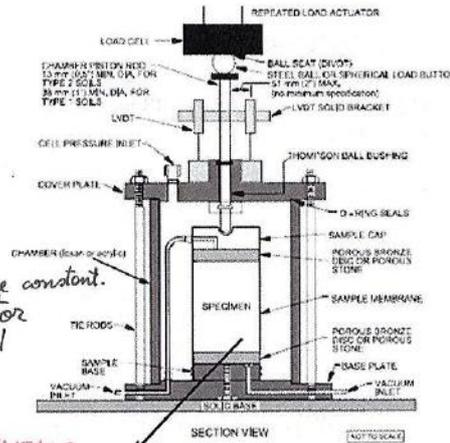
Two confinement conditions

- Constant Cell Pressure (CCP) \oplus deviator stress that pulse!
- Variable Cell Pressure (VCP) cycle

pulse/cycle the confining and deviator

it's time depending

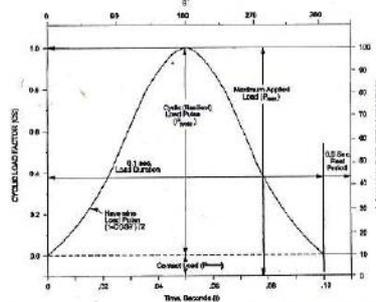
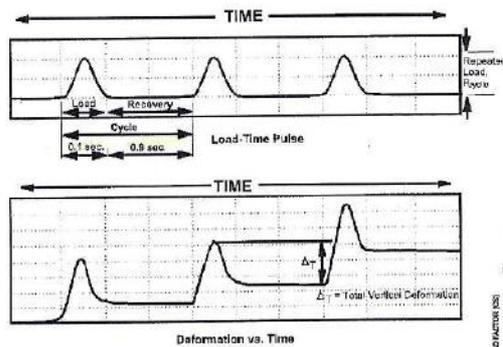
SNELLO SLENDER SPECIMEN ($H = 2D$)
 $\phi = 200\text{mm}$



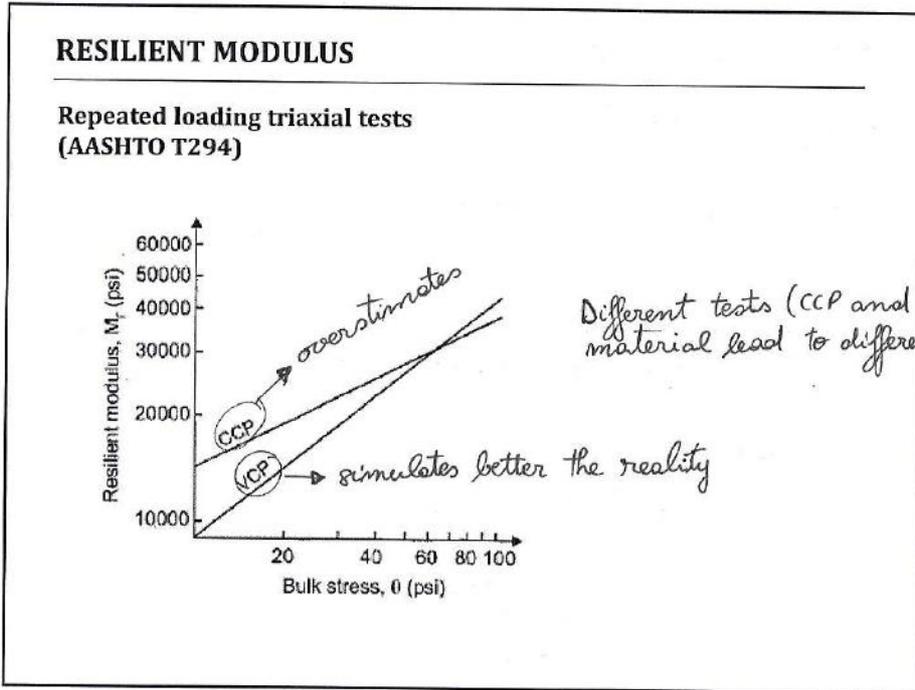
RESILIENT MODULUS

Repeated loading triaxial tests (AASHTO T294)

1) Apply pulses



RESILIENT \approx ELASTIC



RESILIENT MODULUS

Repeated loading triaxial tests
(AASHTO T294)

PERMANENT DEFORMATION

Evaluation of behaviour with respect to rutting $\longrightarrow \epsilon_p = \epsilon_d A \cdot N^{-B}$

\downarrow ORMAIAMENTO

SOTTOFONDO

RESILIENT MODULUS

Models

Fine cohesive materials

Thompson - Elliott

$$M_R = k_1 + k_3 (k_2 - \sigma_d) \quad \text{con } \sigma_d < k_2$$

$$= k_1 + k_4 (k_2 - \sigma_d) \quad \text{con } \sigma_d > k_2$$

Materials are very shear sensitive

∃ 2 linear approximated relationships
(guarola argilla di Doncallotta)

"Stress - softening"

the

COMPRESSIBILITY

Edometric tests

- Totally saturated conditions
- Partially saturated conditions

↓

- Axial load applied to specimen;
- Settlement; → *measure settlements that occur in time.*
- Measurement of displacements.

SEDIMENTO DI ASSETTAMENTO

Pressure increase: $p_0 \rightarrow p_0 + \Delta p$

↓

$e_0 \rightarrow e$

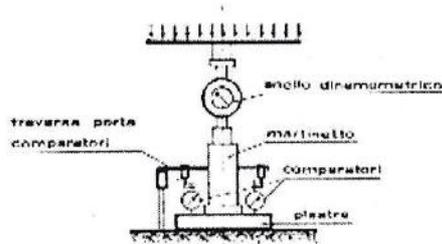
ex for embankments

$$a_v = \frac{e_0 - e}{\Delta p}$$

COMPRESSIBILITY COEFFICIENT

BERING CAPACITY

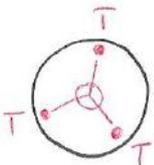
Plate loading test *PROVA DI CARICO SU PIASTRA*



EQUIPMENT

Circular metal plate *placed on top of the surface*
 Hydraulic actuator → ⊕ *CONTRAST = back part of a heavy truck.*
 Transducers (usually 3) *TRASDUTTORE*

fixed to an underformable support far away from the plate ⇒ so they are suspended.



BEARING CAPACITY

Plate loading test

TEST

1. Levelling of surface and plate positioning
2. Set up of actuator and counterweight (e.g. rear axle of heavy vehicle)
3. Set-up of transducers arranged at 120° with arms fixed to supporting beam (supports resting at at least 1 m from plate)
4. Imposition of given load/pressure values and reading of corresponding displacements (stabilization of readings: difference smaller than 0.02 mm after 1 minute)

DIN ≠ Italian
 German

→ For each pressure steps I have to take a reading, that must be stable in time. If it is < 0.02 mm after 1 min ⇒ go c. If it's > 0.02 mm after 1 min ⇒ wait another 1 mi

LOAD → INSTANTANEOUS SETTLEMENT ⊕ TIME-DEPENDENT SETTLEMENT.

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BEARING CAPACITY

REVIEW

Behaviour of soil under loading can be described by referring to two main models

BOUSSINESQ

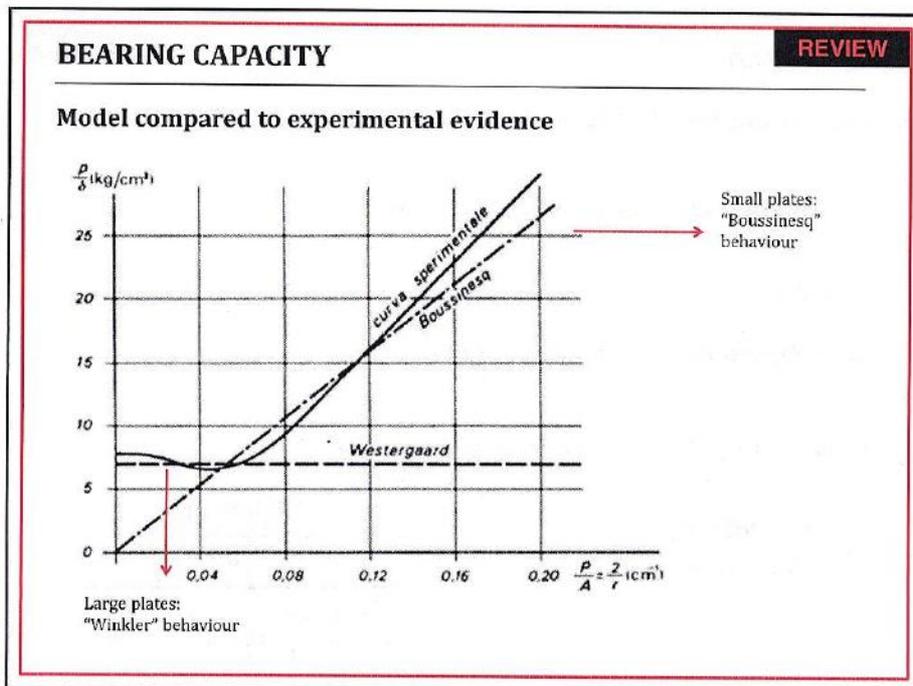
→ Soil is considered as a elastic, homogeneous and isotropic half-space

$$p = \frac{E}{1-\nu^2} \frac{2\delta}{\pi \cdot r}$$

WINKLER

→ Soil is considered as a bed of independent elastic springs

$$p = k \cdot \delta$$



10/10/2017

BEARING CAPACITY

Standard CNR n. 146/1992

$$M_d = \frac{\Delta p}{\Delta \delta} \cdot D$$

↓

Deformation modulus

Test with plate D = 30 cm

⇒ **Control**

(applicable to all parts of earthworks)

BEARING CAPACITY

Benkelmann beam (CNR n. 141/1992)

Measurements are performed by considering the displacement of a point under to the action of a moving vehicle of known characteristics (which gets closer and then leaves).

Total displacment = d (recovered) + p (permanent)

$$M_d = \frac{84}{d}$$

Empirical correlation between Benkelmann test and plate loading test

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BEARING CAPACITY

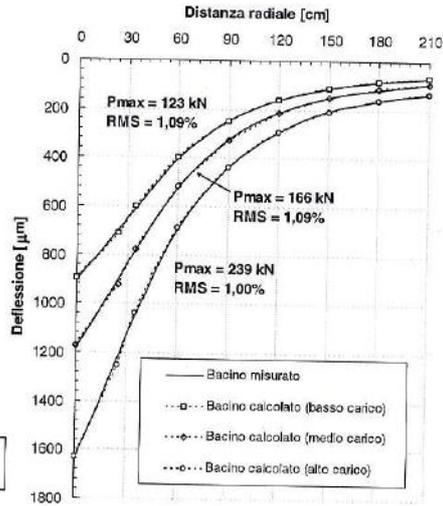
Falling Weight Deflectometer (FWD)

Mechanical characteristics of subgrade (E_s) or pavement (E_i) are derived from the deflection basin provided that the cross-section is known (**Back-calculation procedure**)

Comparison between measured and calculated basin:

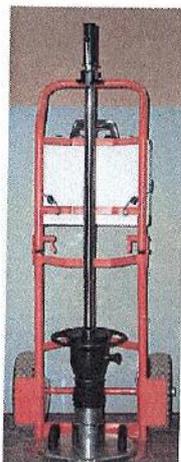
$$RMS(\%) = 100 \cdot \sqrt{\frac{1}{9} \sum_{i=1}^9 \left(\frac{d_{ci} - d_{mi}}{d_{mi}} \right)^2}$$

TREATED IN DETAIL IN THE PART ON PAVEMENTS (STRUCTURAL EVALUATION)



BEARING CAPACITY

Light Weight Drop Tester (LWDT)



Very useful equipment, easy to handle and to use, for the quick control of earthworks (embankments, subgrades, foundations)



$$E_{s,din} = \frac{22,5}{d}$$

From Boussinesq

16/10/2017



POLITECNICO DI TORINO
Master Course
in Civil Engineering
2017-18



Construction of Roads, Railways and Airports (01RVMMX)

EARTHWORKS
Construction of the road prism



Construction of the road prism

Carried out by means of earthworks.

The following activities are usually performed:

- CLEARING AND GRUBBING
- REMOVAL OF TOPSOIL
- EXCAVATIONS (opening of roadway, preparation of foundations for embankments and other elements)
- EMBANKMENT CONSTRUCTION - SUBGRADE
- FILL

ACTIVITIES CLEARING CONSTRUCTION SITE.

→ separated, can be useful for slopes

FOR CUT SECTIONS, NOT ONLY ALSO REFILL w/ some topsoil

→ timber, # types

16/10/2017

Construction of the road prism

EXCAVATION

- opening of roadway;
- formation of pavement section in cut sections;
- remediation of embankment foundation, including formation of transverse steps (if transverse slope > 15%);

start to excavate in cut section to reuse soil

The diagrams illustrate the progressive stages of road prism excavation. The 'PROFILE' shows the initial ground surface. The '1st' stage shows the initial cut. The '2nd', '3rd', and '4th' stages show the deepening and widening of the cut, with the road prism being formed on the lower slopes.

Construction of the road prism

EQUIPMENT (EXCAVATION, LOADING, TRANSPORT)

The diagrams illustrate the various pieces of equipment used in road prism construction:

- DOZER (APRIPISTA)**: Used for initial earthmoving.
- EXCAVATOR**: Used for deepening and widening the cut.
- MOTOR-SCRAPER (RUSPA)**: *cuts away material and also transports*. It is used for leveling and transporting material.
- WHEEL LOADER (PALA CARICATRICE)**: *to put material in tracks*. Used for loading material onto transport vehicles.
- DUMPER**: *tipover dumper*. Used for transporting material to the construction site.
- GRADER (LIVELLATRICE)**: *to provide proper grade to surface*. Used for final grading and leveling of the road surface.

push the material (handwritten note pointing to the dozer)

water for soil (handwritten note pointing to the motor-scraper)

to provide proper grade to surface (handwritten note pointing to the grader)

Construction of the road prism

EMBANKMENT FOUNDATION - Compressible soils

If predicted settlements of the embankment foundation are greater than **15 cm**, the Contractor will prepare a detailed workplan for their measurement and monitoring in time.

Embankment construction will be scheduled in order to have a residual settlement (still to occur) at the end construction less than of **10%** of totale estimated settlement and in any case lower than **5 cm**.

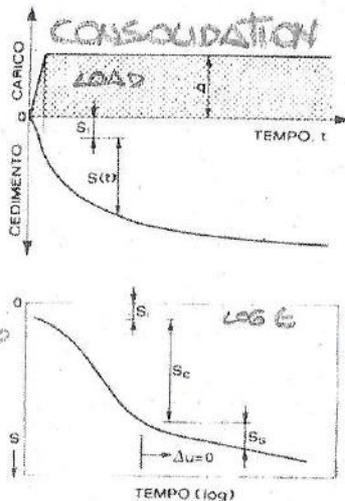
(CIRS Technical Specifications)

SETTLEMENT OCCURRING IN TIME -
LITTLE PART, SMALLEST POSSIBLE

Construction of the road prism

Terzaghi theory

EMBANKMENT FOUNDATION - Settlements



$$S = S_i + S_c(t) + S_s(t)$$

- Immediate settlement S_i - due to load application (undrained conditions)
- Consolidation settlement $S_c(t)$ - due to the progressive load transfer to soil particles
- Secondary settlement $S_s(t)$ - due to viscous strains ($\Delta u = 0$)

In the case of coarse-grained soils no consolidation: initial and secondary.

No settlement embankment
xk already compacted & basic material
won't be changing in shape

calculate settlement
Boussinesq

IMMEDIATE SETTLE S_i
CONSOLIDATION S_c \rightarrow ^{equal} from water to soil
SECONDARY S_s \rightarrow VISCIOUS STRAINS

16/10/2017

Construction of the road prism

COMPRESSIBLE SOILS - Vertical drains

Often combined with preloading

Function of drains
 ↓
 Modify drainage path (radial) and reduce consolidation time

COLUMN ATTRACTS WATER

RADIO FLOW OF THE WATER

TYPES

- Sand drains (natural)
- Precast drains

DIAMETER → affects on function of system

CHOOSE - APPROPRIATE WATER AND SOIL

COLUMNS FILLED WITH SAND
 ↓
 DRAINAGE FREE

Construction of the road prism

COMPRESSIBLE SOILS - Sand drains (natural)

Vertical drilling followed by filling with selected sand

Particle size distribution (ASTM)

| Sieve opening [mm] | Passing [%] |
|--------------------|-------------|
| 4.75 (4 ASTM) | 85 + 100 |
| 1.18 (16 ASTM) | 40 + 85 |
| 0.300 (50 ASTM) | 5 + 30 |
| 0.150 (100 ASTM) | 2 + 10 |
| 0.075 (200 ASTM) | 0 + 3 |

FOR ANTICIPATORY COVER AND HIGH DRAINAGE LEVEL

LOW, SO NO CAPILLARITY

One can inject air, water, concrete.

Diameters go from 0.4 m = 40 cm to 2.5 m.

Usually use in industrial ports, airports because it's expensive.

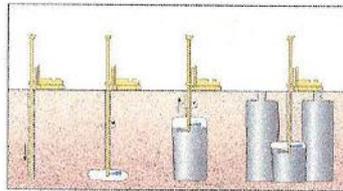
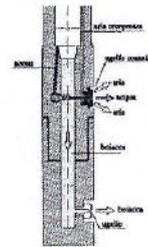
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Construction of the road prism

COMPRESSIBLE SOILS - Column treatment

| Sistema | Fluido | Pressione (MPa) | Velocità getto (m/s) | D (m) |
|-------------------------------|--------------------|-----------------|----------------------|-------------|
| Monofluido | Bolacca di cemento | 20 + 40 | 100 + 250 | 0.40 + 0.60 |
| Bifluido (Jumbo special pile) | Bolacca di cemento | 25 + 40 | 100 + 200 | 0.80 + 1.60 |
| | Aria | 0.7 + 1 | > 330 | |
| Trifluido (Kajima) | Bolacca di cemento | 2 + 6 | 50 + 80 | 0.80 + 2.50 |
| | Aria | 0.7 + 1.7 | > 330 | |
| | Acqua | 40 + 60 | 350 + 500 | |

JET-GROUTING

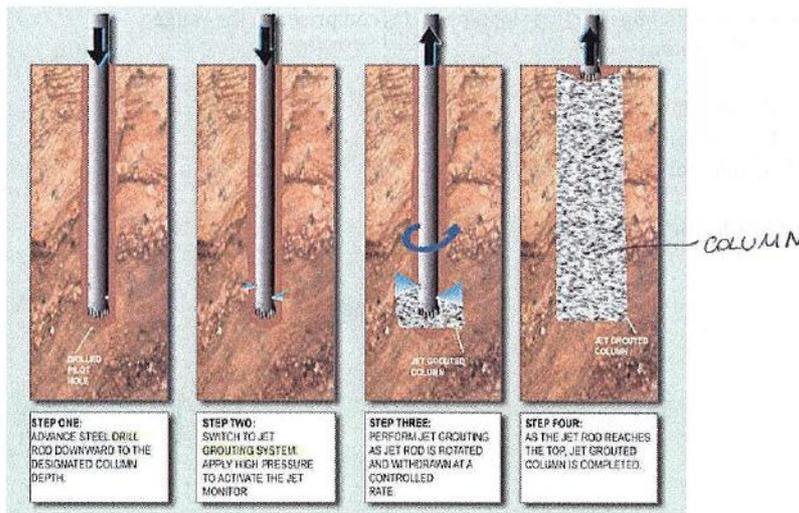


Construction of the road prism

COMPRESSIBLE SOILS - Column treatment

JET-GROUTING

Drilling operation



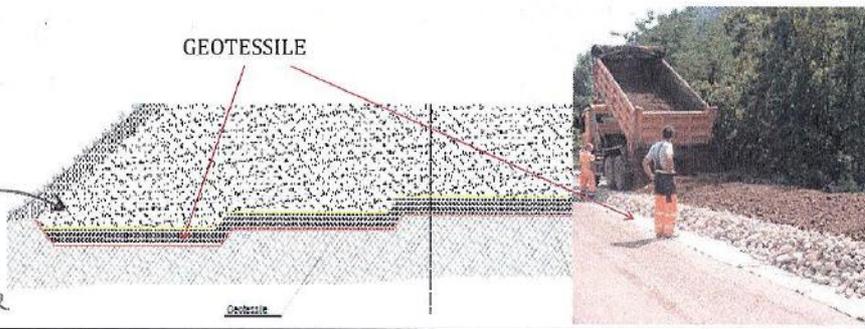
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Construction of the road prism

EMBANKMENT FOUNDATION - Anti-capillary layers

Composed of natural material, thickness usually of the order of 30-50 cm, constituted by granular soil (gravel), with particles sizes comprised between 2 and 50 mm, with a percent passing 2 mm sieve not greater than 15% and percent passing 0,075 mm sieve non greater than 3%.
 Absence of unstable components (soluble, degradable, sensitive to freeze/thaw) and organic residues; the use of crushed or recycled materials is admitted.

CLEAN GRAVEL



GRANULAR MATERIAL

- must be very durable
- expensive
- must have low fine fraction.

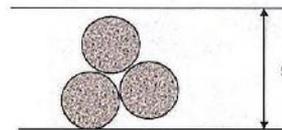
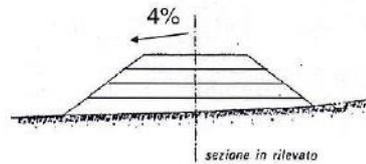
Construction of the road prism

EMBANKMENTS

Construction operations:

- thickness of layers depends upon characteristics of materials and available equipment;
- thickness of layers not smaller than twice the maximum particle size of employed soil ($s > 2 D_{max}$); in any case, $D_{max} < 300$ mm (coarser particles should be discarded)
- inclined working planes for water runoff **TRANSVERSE SLOPE**
- construction of a layer depends on preliminary verification of underlying layers (**bearing capacity, in situ density**)

↳ NO TESTS IN SITU

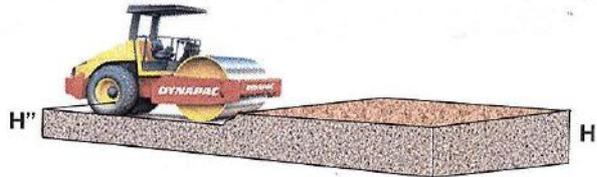


coarse material can't be placed in thin layers. Particles not bigger than $\phi = 300$ mm

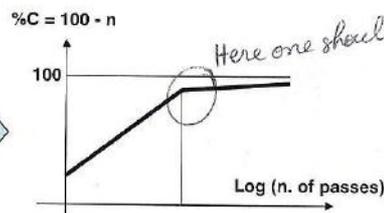
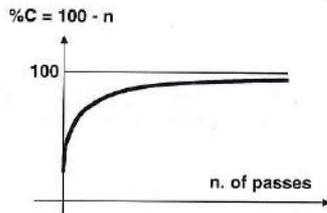
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Construction of the road prism

GENERAL PRINCIPLES OF IN SITU COMPACTION



%C = percent compaction
n = porosity



Here one should have a good compaction

Construction of the road prism

GENERAL PRINCIPLES OF IN SITU COMPACTION

Static compaction

Based on the action of dead weight of equipment which translates into vertical stresses. Internal friction is overcome and soil volume is reduced.

Limited effect in depth (effects typically extend down to 20 cm). *in general*
Smooth static compaction is useful for finishing operations after oscillatory/vibratory compaction (limits the risks of surface disintegration).

OVERCOMING INT. FRICTION ←

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The DIRECTION of the force changes in time following the law

Construction of the road prism

DYNAMIC COMPACTION

It follows: ACCELERATION OF DRUM?

$a_T = \frac{M_e \cdot \omega^2}{m_T}$ $\xrightarrow{F_c \text{ that we know now.}}$ Drum acceleration

$a_{T,V} = \frac{M_e \cdot \omega^2}{m_T} \cos(\omega t)$ $\xrightarrow{\text{Vertical component of acceleration}}$

INTEGRATE twice

$v_{T,V} = \int_0^t \frac{M_e \cdot \omega^2}{m_T} \cos(\omega t) dt = \frac{M_e \cdot \omega}{m_T} \text{sen}(\omega t)$

$s_{T,V} = \int_0^t \frac{M_e \cdot \omega}{m_T} \text{sen}(\omega t) dt = -\frac{M_e}{m_T} \cos(\omega t)$

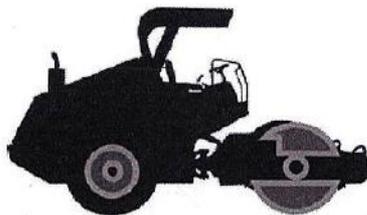
$A_T = |\max s_{T,V}| = \frac{M_e}{m_T} = \frac{F_c}{m_T \cdot \omega^2}$ **Maximum theoretical oscillation amplitude of a «suspended» drum IDEAL**

ROLLER: $m_T = \text{mass of drum}$ } amplitude of vibration (oscillation) \rightarrow in horizontal and vertical direction.
 M_e, r } not in contact with soil

Construction of the road prism

DYNAMIC COMPACTION

Drum-soil interaction model



SPRINGS
 DASHPOTS ammortizzatore

$$\begin{aligned} & -m_f \ddot{z}_f \\ & |m_d \ddot{z}_d \\ & \downarrow m_d \dot{e}^{\omega t} \Omega^2 \cos(\Omega t) \\ & | (m_d' + m_f) g \\ & \downarrow F_s = k_s z_d + c_s \dot{z}_d \end{aligned}$$

in contact with soil



Construction of the road prism

DYNAMIC COMPACTION

Lundberg model

Rigid body on elastic homogeneous and isotropic support

DISPLACEMENT z_d

LOADING F_s

LENGTH L

constant b

$$z_d = \frac{2 \cdot (1 - \nu^2) \cdot F_s}{\pi \cdot E \cdot L} \left(1,8864 + \ln \frac{L}{b} \right)$$

$b = \sqrt{\frac{16 \cdot R \cdot (1 - \nu^2)}{\pi \cdot E \cdot L} \cdot F_s}$ Contact width of body (drum)

Parameter used for the control of compaction characteristics

Handwritten note: $z_d \propto F_s$ and at a given geometry is controlled by E_d

Construction of the road prism

INTELLIGENT COMPACTION \equiv *CCC continuous Compaction Control.*

Several compactors have a measurement system which allows real-time monitoring of mechanical properties of soil and the consequent modification of the compaction procedure in order to obtain required final results (**Intelligent Soil Compaction**)

Handwritten note: have a mapping of the area

Handwritten note: measures the E

CHART

F_s and z_d measured by equipment

Estimate of E (E_{VIB})

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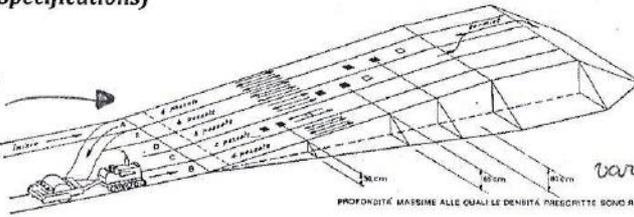
Construction of the road prism

SITE TRIALS

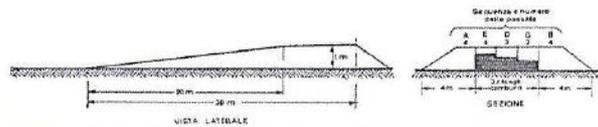
Necessary for all major construction works.
 The purpose is to define and validate the routine working technique in terms of employed equipment and layer thicknesses.
 End results have to be checked in terms of dry density and bearing capacity.

(CIRS Technical Specifications)

STRIPS with different characteristics



Have at least 1 parameter changing to see what happens



Construction of the road prism

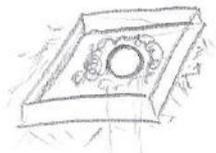
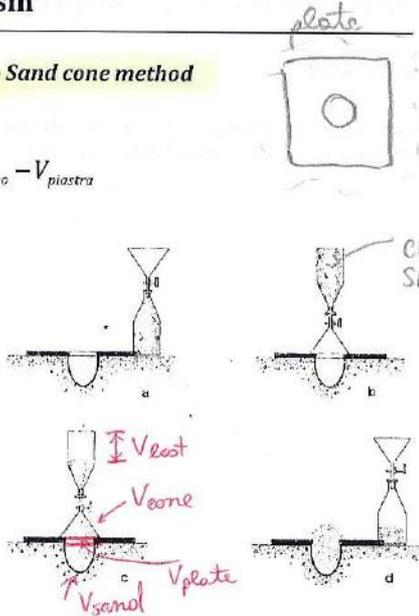
MEASUREMENT OF IN SITU DENSITY - Sand cone method

Volume of void $V = \frac{m_1 - m_2}{\gamma_{s, mucchio}} - V_{Cano} - V_{piastra}$

Dry density $\gamma_s = \frac{m_3}{1 + \frac{w}{100} V}$

In cui:

- m_1 = mass of the full container
- m_2 = mass of the empty container
- m_3 = mass of extracted sample



CALIBRATED SAND

$V_{leat} = V_{cone} + V_{plate} + V_{sand}$
 known

PROCTOR

DRY DENSITY

calculated after having some size of particles

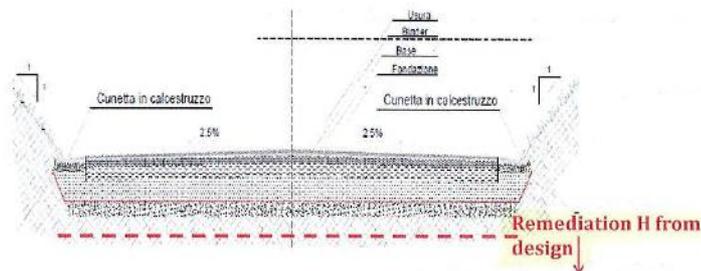
to compare DRY DENSITIES we have to take out some particles from SAND CONE METHOD.

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Construction of the road prism

SUBGRADE

Soil volume in which the effects of traffic loading are non-negligible; it is the zone of transition between embankment/ground and pavement.



- Substitution of in situ material
- Stabilization of in situ material

Construction of the road prism → Closer to the loads :

SUBGRADE - Employed soils

Evenness of pavement laying surface leads to exclusion of particles greater than $D=100$ mm;

Use of granular soils, well-distributed, preferably composed of crushed particles, with low fine content (percent passing the 0,075 mm sieve lower than 12%) and not plastic ($PI < 6$).

Materials belonging to groups A1-a are of premium quality.

Alternative materials:

- Soils of groups A1-b;
- Soils of groups A2-4 ed A2-5, with percent passing the 0.075 mm sieve greater than 12%, preliminarily subjected to stabilization with cement or cement-lime;
- Soils of groups A2-6 ed A2-7 with a percentage of fines greater than 5% preliminarily subjected to stabilization with lime or cement-lime;
- Silts of groups A4 ed A5 if subjected to cement-lime stabilization, and clays of groups A6 ed A7, with limited plasticity ($PI < 25\%$), if subjected to lime stabilization.

- low fine content
- non plastic
- A1-a, A1-b should be used
- A2 ÷ A5 must be stabilized

24/10/2017



POLITECNICO DI TORINO
Master Course
in Civil Engineering
2017-18



Construction of Roads, Railways and Airports (01RVMMX)

EARTHWORKS
Equipment



EARTHWORKS

DEFINITIONS

L'attività di movimento terra (MT), di norma, si esplica attraverso l'impianto di aree di cantiere, finalizzate alla realizzazione di opere civili (dalla costruzione di edifici fino alle grandi infrastrutture)

Risulta, quindi, di fondamentale importanza, per la riuscita di un lavoro, predisporre ed attivare un CANTIERE MECCANIZZATO per la lavorazione delle terre che sia funzionalmente rispondente alle esigenze tecnico-economiche del lavoro da eseguire.

La CANTIERIZZAZIONE DELL'OPERA è un PROGETTO che ha come risultato:

- **scelta dei singoli mezzi meccanici** occorrenti per ogni lavorazione, determinandone le relative caratteristiche: tipo, potenza, quantità o numero; → EACH UNIT / MACHINE
- **determinazione del ciclo di lavoro** delle singole macchine e del ciclo delle lavorazioni effettuate da più macchine fra loro interdipendenti; → CONSIDER THE INTERACTIONS BETWEEN MACHINES
- **predisposizione di diagrammi di lavorazione** da cui derivare lo schema dell'organizzazione generale del cantiere. → DIAGRAMS

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EARTHWORKS

TRANSFORMATION COEFFICIENTS

In order to identify the equipment to employ for earthworks, it is necessary to know the ratio between the various volumes, defined by means of **transformation coefficients**.

γ_b , γ_s and γ_c : densities corresponding to bank, loose and compacted conditions

The following relationships hold (for a given, constant mass P of soil):

SWELL FACTOR $\rightarrow f_r$ (from bank to loose) [%] : "RIGONFIAMENTO"

$$f_r = \left(\frac{V_s - V_b}{V_b} \right) \cdot 100 = \left(\frac{V_s}{V_b} - 1 \right) = \left(\frac{\gamma_b}{\gamma_s} - 1 \right) \cdot 100$$

LOADING FACTOR $\rightarrow f_c$ (from loose to bank) :

$$f_c = \frac{V_b}{V_s} = \frac{\gamma_s}{\gamma_b}$$

moreover: $f_r = \left(\frac{1}{f_c} - 1 \right) \cdot 100$

EARTHWORKS

TRANSFORMATION COEFFICIENTS/1

| WEIGHT* OF MATERIALS | LOOSE | | BANK | | LOAD FACTORS |
|--------------------------------------|-------------------|--------------------|-------------------|--------------------|--------------|
| | kg/m ³ | lb/yd ³ | kg/m ³ | lb/yd ³ | |
| Basalt | 1960 | 3300 | 2370 | 5000 | 0.67 |
| Bauxite, kaolin | 1420 | 2400 | 1900 | 3200 | 0.75 |
| Caliche | 1250 | 2100 | 2260 | 3900 | 0.55 |
| Canolite, Washburne | 1530 | 2750 | 2200 | 3700 | 0.74 |
| Clayais | 560 | 950 | 680 | 1480 | 0.66 |
| Clay - Natural bed | 1660 | 2900 | 2020 | 3400 | 0.82 |
| Dry | 1480 | 2500 | 1940 | 3100 | 0.81 |
| Wet | 1660 | 2900 | 2080 | 3500 | 0.80 |
| Clay & gravel - Dry | 1420 | 2400 | 1660 | 2800 | 0.85 |
| Wet | 1540 | 2600 | 1840 | 3100 | 0.85 |
| Coal - Anthracite, Raw | 1190 | 2000 | 1600 | 2700 | 0.74 |
| Washed | 1100 | 1850 | | | 0.74 |
| Ash, Bituminous Coal | 530-650 | 900-1100 | 590-690 | 1000-1500 | 0.93 |
| Bituminous, Raw | 750 | 1600 | 1280 | 2150 | 0.74 |
| Washed | 820 | 1400 | | | 0.74 |
| Decomposed rock - | | | | | |
| 75% Rock 25% Earth | 1980 | 3300 | 2750 | 4700 | 0.70 |
| 50% Rock 50% Earth | 1720 | 2900 | 2290 | 3850 | 0.75 |
| 25% Rock 75% Earth | 1570 | 2650 | 1950 | 3300 | 0.80 |
| Earth - Dry packed | 1510 | 2550 | 1900 | 3200 | 0.80 |
| Wet excavated | 1600 | 2700 | 2020 | 3400 | 0.75 |
| Loam | 1250 | 2100 | 1540 | 2600 | 0.81 |
| Granite - Broken | 1660 | 2900 | 2730 | 4600 | 0.61 |
| Gravel - Pitrun | 1930 | 3250 | 2170 | 3650 | 0.89 |
| Dry | 1510 | 2550 | 1690 | 2850 | 0.89 |
| Dry 6-50 mm (1/4"-2") | 1630 | 2850 | 1900 | 3200 | 0.89 |
| Wet 6-50 mm (1/4"-2") | 2020 | 3400 | 2260 | 3900 | 0.89 |
| Gypsum - Broken | 1810 | 3050 | 2170 | 3580 | 0.57 |
| Crushed | 1500 | 2700 | 2790 | 4700 | 0.57 |
| Hematite, iron ore, high grade | 1910-2450 | 4000-5400 | 2120-2900 | 4700-5400 | 0.85 |