



Corso Luigi Einaudi, 55 - Torino

**Appunti universitari**

**Tesi di laurea**

**Cartoleria e cancelleria**

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**Rilegature**

NUMERO: 1941A -

ANNO: 2016

# **A P P U N T I**

STUDENTE: Prette Arianna

MATERIA: Scienza delle costruzioni - prof. Surace

Il presente lavoro nasce dall'impegno dell'autore ed è distribuito in accordo con il Centro Appunti.

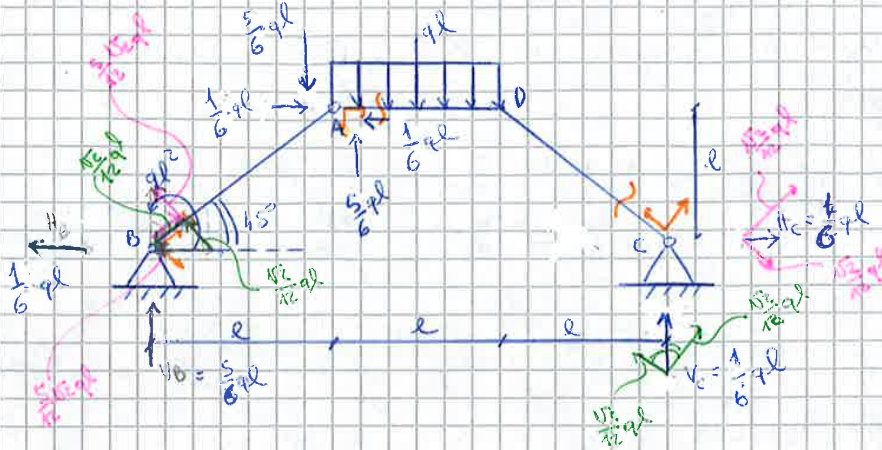
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ATTENZIONE: QUESTI APPUNTI SONO FATTI DA STUDENTIE NON SONO STATI VISIONATI DAL DOCENTE.  
IL NOME DEL PROFESSORE, SERVE SOLO PER IDENTIFICARE IL CORSO.

TEMA D'ESAME

6/9/05

ES. 1



1) REAZIONI VINCENTI:

→  $H_B + H_C = 0 \quad (H_C) = -\frac{1}{6}ql + \frac{1}{6}ql$

↑  $V_B + V_C - ql = 0 \quad \rightarrow (V_B) = \frac{5}{6}ql + \frac{1}{6}ql = \frac{5}{6}ql + \frac{1}{6}ql = \frac{5}{6}ql$

⊙  $M(B) \rightarrow ql^2 - ql \cdot \frac{3}{2}l + V_C \cdot 3l = 0 \rightarrow V_C = \frac{\frac{2}{3}ql^2 + \frac{3}{2}ql^2}{3l}$

$(V_C) = \frac{+\frac{1}{2}ql^2}{3l} = -\frac{1}{6}ql + \frac{1}{6}ql$

equazione equilibrio corpo 1:

⊙  $M(A) = -V_B \cdot l + H_B \cdot l + ql^2 = 0$

$-\frac{5}{6}ql^2 + H_B \cdot l + ql^2 = 0 \quad H_B = \frac{(\frac{1}{6}ql^2 + \frac{5}{6}ql^2)}{l}$

$(H_B) = \frac{\frac{1}{6}ql^2}{l} = \frac{1}{6}ql - \frac{1}{6}ql$

SOLLECITAZIONI

TRAVERSA BA:

←  $N = \frac{1}{6}ql \cdot \frac{\sqrt{2}}{2} - \frac{5}{6} \frac{\sqrt{2}}{2} ql \quad \rightarrow N = \frac{1\sqrt{2}}{12}ql - \frac{5\sqrt{2}}{12}ql = -\frac{4\sqrt{2}}{12}ql = -\frac{\sqrt{2}}{3}ql$

↑  $T = \frac{\sqrt{2}}{2} \cdot \frac{1}{6}ql + \frac{\sqrt{2}}{2} \cdot \frac{5}{6}ql \quad \rightarrow T = \frac{\sqrt{2}}{12}ql + \frac{5\sqrt{2}}{12}ql = \frac{\sqrt{2}}{2}ql$

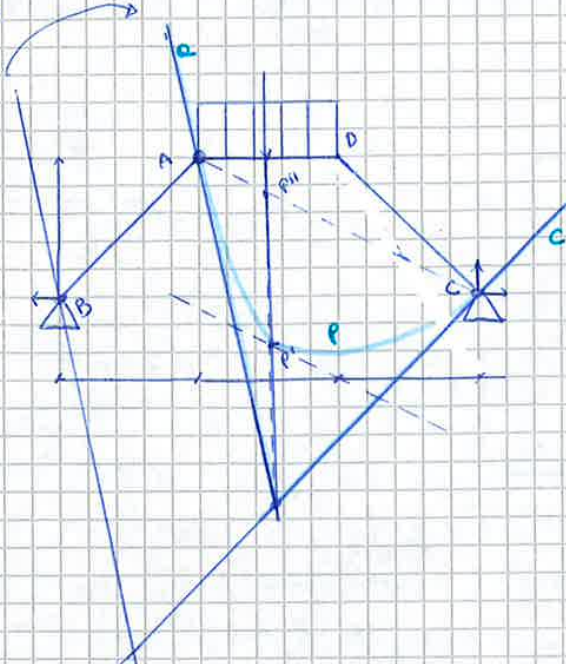
⊙  $M = -ql^2 + \frac{\sqrt{2}}{12}ql \cdot z + \frac{5\sqrt{2}}{12}ql \cdot z = -ql^2 + \frac{\sqrt{2}}{2}qlz \quad M(B) = M_B = -ql^2$   
 $\rightarrow M(A) = -ql^2 + \frac{\sqrt{2}}{2}ql \cdot l\sqrt{2}$

$M_A = M(B) = -ql^2 + ql^2 = 0$

2)

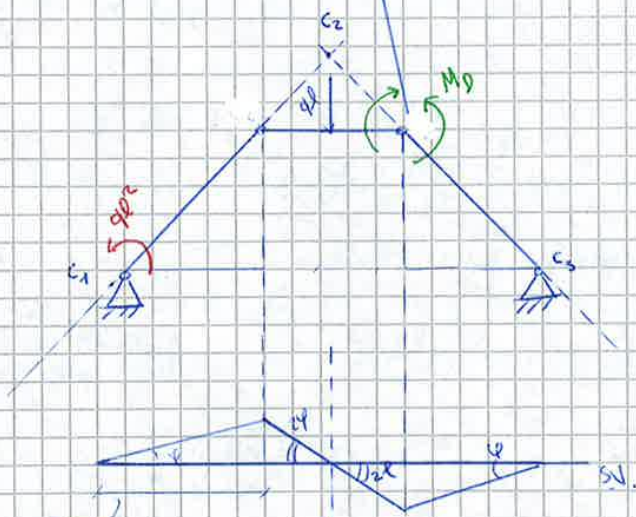
perché deve passare per la colonna

la trave in A



tratto	cdp
AB	retta a
AD	parabola p
DC	<del>parabola</del> retta c

3)



S.O.  
NB.  
→ centro di rotazione  
essenziale = spostamento nullo!

$$2y = \theta \cdot \frac{l}{2}$$

$$\theta = 2y$$

$$q l^2 \cdot y + q l \cdot 0 + M_D \cdot y + M_D \cdot 2y = 0$$

$$q l^2 y + M_D 3y = 0 \quad \rightarrow \quad M_D = - \frac{q l^2}{3}$$

$$x_1 = \frac{-2l^2 \Delta T}{3EI} = -2l^2 \cdot \frac{3EI}{8l} = -\frac{3EI}{4l} \Delta T$$

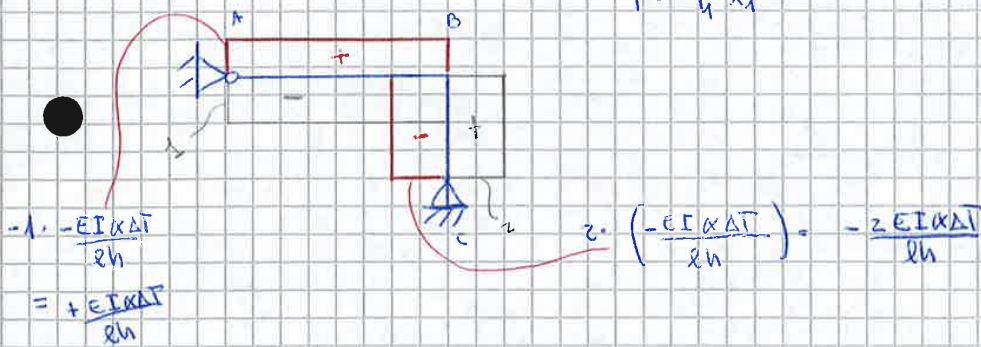
$$\int \frac{M^2}{EI} dz = \frac{1}{EI} \cdot \frac{8}{3} l^3 + \frac{1}{EI} \frac{1}{6} 8l^2 = \frac{1}{EI} \left( \frac{16l^3 + 8l^3}{6} \right) = \frac{1}{EI} \left( \frac{24l^3}{6} \right) = \frac{4l^3}{EI}$$

$$\textcircled{x_1} = \frac{+2l^2 \Delta T}{\frac{24l^3}{EI}} = + \frac{EI \Delta T}{2l} = - \frac{EI \alpha \Delta T}{lh} \quad \text{perché:} \quad \Delta T = - \frac{2\alpha \Delta T}{h}$$

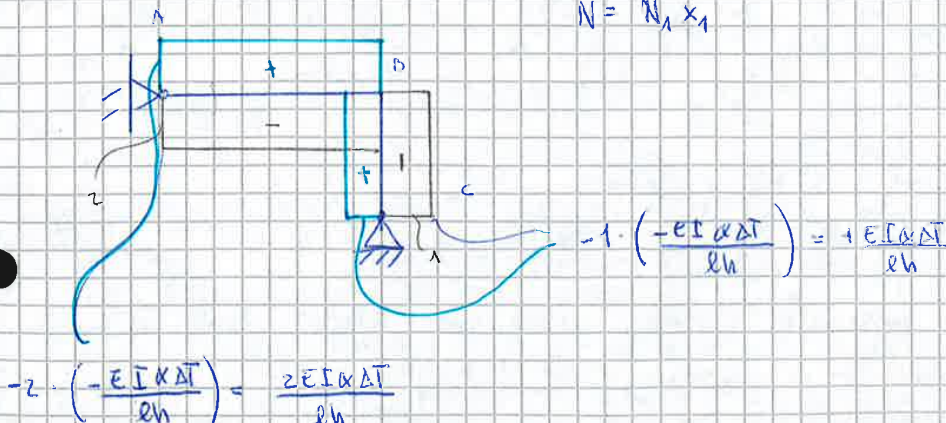
diagramma momento  $M = M_1 x_1$



$$T = T_1 x_1$$



$$N = N_1 x_1$$



$$\sigma_{\tau} = \frac{N}{A} + \frac{M_x}{I_x} y$$

$$\sigma_{\tau \max} = \frac{N_B}{A} + \frac{M_B}{I_x} y$$

$$A_{\text{tot}} = h \cdot \delta + z \cdot \delta \left( \frac{h}{z} \right) = 2h\delta$$

$$\sigma_{\tau \max} = \frac{\frac{2EI\alpha\Delta T}{h}}{\frac{\delta h^3}{3}} \cdot \frac{h}{z} + \frac{\frac{2EI\alpha\Delta T}{zh}}{zh\delta}$$

$$\sigma_{\tau \max} = 3 \frac{EI\alpha\Delta T}{\delta h^3} + \frac{EI\alpha\Delta T}{\delta l h^2}$$

$$\sigma_{\tau \max} = \frac{3EI\alpha\Delta T}{\delta h^3} \left( 1 + \frac{h}{3l} \right) = EI\alpha\Delta T \left( 1 + \frac{h}{3l} \right)$$

ma  $h \ll l$

$$\sigma_{\tau \max} \cong EI\alpha\Delta T$$

contributo di  $N$  è molto inferiore a quello del momento flettente

TRATTO EB

$$\leftarrow N = -2ql + \frac{7}{2}ql = \frac{-4ql + 7ql}{2} = \frac{3ql}{2}$$

$$\uparrow T = -\frac{3}{2}ql$$

$$\begin{aligned} \curvearrowright M &= -\frac{3}{2}ql \cdot z + \frac{7}{2}ql \cdot 2l - 2ql \cdot l & M(z) = M_c &= \frac{7}{2}ql^2 - 2ql^2 \\ & & &= \frac{7ql^2 - 4ql^2}{2} = \frac{3ql^2}{2} \\ M_0 = M(l) &= -\frac{3}{2}ql \cdot l + \frac{7}{2}ql \cdot 2l - 2ql^2 \\ &= -\frac{3}{2}ql^2 + \frac{7}{2}ql^2 - 2ql^2 = \frac{-3 + 7 - 4}{2} ql^2 = 0 \end{aligned}$$

TRATTO DC

$$\leftarrow N = -\frac{5}{4}ql$$

$$\uparrow T = \frac{1}{4}ql$$

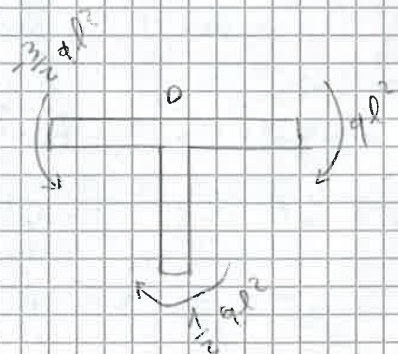
$$\begin{aligned} \curvearrowright M &= \frac{1}{4}ql \cdot z & M(z) = 0 = M_c \\ & & M(2l) = M_D &= \frac{1}{4}ql \cdot 2l = \frac{1}{2}ql^2 \end{aligned}$$

TRATTO DF

$$\leftarrow N = 0$$

$$\uparrow T = ql$$

$$\begin{aligned} \curvearrowright M &= ql \cdot z & M(z) = M_F &= 0 \\ & & M(l) = M_D &= ql^2 \end{aligned}$$



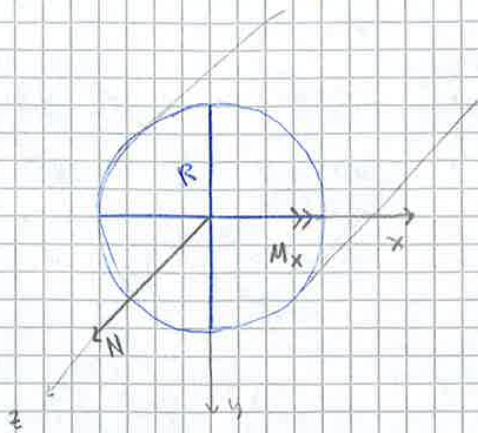
TRATTO ED

$$\leftarrow N = -\frac{ql}{2}$$

$$\uparrow T = -\frac{3}{2}ql$$

$$\begin{aligned} \curvearrowright M &= -\frac{3}{2}ql \cdot z & M(z) = M_D &= 0 \\ & & M(l) = M_D &= -\frac{3}{2}ql^2 \end{aligned}$$

La sezione dove il momento flettente è max è la F. ( $M(\frac{7}{4}l)$ )  
 che si trova a  $\frac{7}{4}l$  da A



$$\sigma_z = \frac{N}{A} + \frac{M}{I_x} y$$

$$I_x = \frac{\pi R^4}{4}$$

massimo

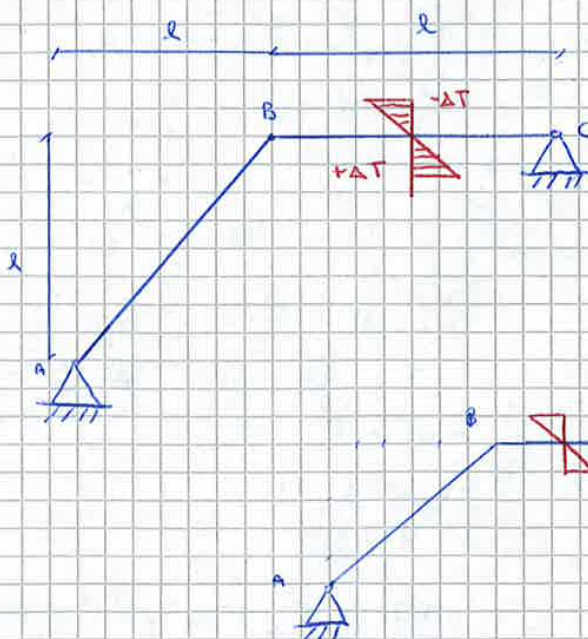
$$\sigma_z = \frac{\frac{3}{2}ql}{\pi R^2} + \frac{\frac{49}{32}ql^2}{\frac{\pi R^4}{4}} \cdot R$$

$$M\left(\frac{7}{4}l\right) = \frac{7}{4}ql \cdot \left(\frac{7}{4}l\right) - \frac{q}{2} \left(\frac{7}{4}l\right) \left(\frac{7}{4}l\right) = \frac{49}{16}ql^2 - \frac{q}{2} \left(\frac{49}{16}l^2\right) = \frac{49}{16}ql^2 - \frac{49ql^2}{32}$$

$$= \frac{98 - 49}{32} ql^2 = \frac{49}{32} ql^2$$

$$\sigma_z = \frac{\frac{49}{32}ql^2 \cdot R}{\frac{\pi R^4}{4}} = \frac{49}{8\pi} \frac{ql^2}{R^3}$$

ES. 2



$$g = 3$$

$$v = 4$$

$g - v = 1$   
 2 volte iperstatica

$$\Delta t = \frac{+2\alpha \Delta T}{h}$$



$$\begin{aligned}
 2) \frac{1}{EI} \int_A^B M_1^2 dz &= \frac{l\sqrt{2}}{6EI} \cdot \left( 0 \cdot 0 + \left(\frac{1}{2}l\right)\left(\frac{1}{2}l\right) + 4\left(\frac{l}{4}\right)\left(\frac{l}{4}\right) \right) \\
 &= \frac{l\sqrt{2}}{6EI} \cdot \left( \frac{1}{4}l^2 + \frac{l^2}{4} \right) = \frac{l\sqrt{2}}{6EI} \cdot \left( \frac{2l^2 + l^2}{4} \right) \\
 &= \frac{l\sqrt{2}}{6EI} \cdot \frac{3l^2}{4} = \frac{3\sqrt{2}l^3}{24EI} = \frac{l\sqrt{2}}{6EI} \cdot \frac{2l^2}{4} = \frac{\sqrt{2}l^3}{12EI}
 \end{aligned}$$

$$\begin{aligned}
 \frac{1}{EI} \int_B^C M_1^2 dz &= \frac{l}{6EI} \left( \frac{1}{2}l \cdot \frac{1}{2}l + 4\left(\frac{l}{4}\right)\left(\frac{l}{4}\right) + 0 \cdot 0 \right) \\
 &= \frac{l}{6EI} \left( \frac{1}{4}l^2 + \frac{l^2}{4} \right) = \frac{l}{6EI} \cdot \frac{1}{2}l^2 = \frac{1}{12} \frac{l^3}{EI}
 \end{aligned}$$

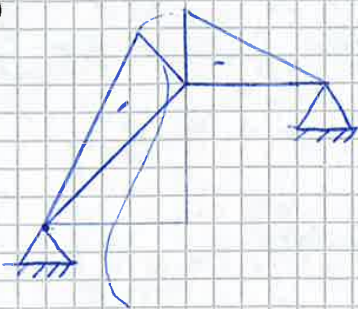
$$\int_S \frac{M_1^2}{EI} dz = \left( \frac{\sqrt{2}}{12} + \frac{1}{12} \right) \cdot \frac{l^3}{EI} = \left( \frac{\sqrt{2}+1}{12} \right) \frac{l^3}{EI}$$

$$\delta_H = \frac{-\frac{l^2}{4} \chi t}{\left(\frac{\sqrt{2}+1}{12}\right) \frac{l^3}{EI}} = -\frac{l^2}{4} \chi t \cdot \frac{12EI}{(\sqrt{2}+1)l^3} = -\frac{3\chi t EI}{(\sqrt{2}+1)l} = -\frac{3(\sqrt{2}-1)EI\chi t}{l}$$

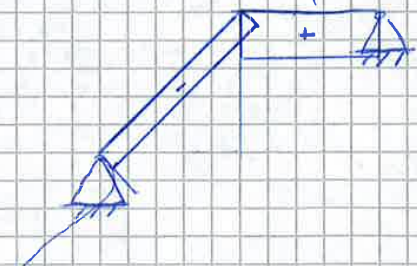
Momento reale:  $M = M_1 \chi_1$

Torquio reale:  $\bar{M} = \chi_1 T_1$

$$-\frac{1}{2} \cdot \frac{-3(\sqrt{2}-1)EI\chi t}{l} = +\frac{3}{2}(\sqrt{2}-1) \frac{EI\chi t}{l}$$



$$\frac{1}{2}l \cdot \left( \frac{-3(\sqrt{2}-1)EI\chi t}{l} \right) = -\frac{3}{2}(\sqrt{2}-1)EI\chi t$$

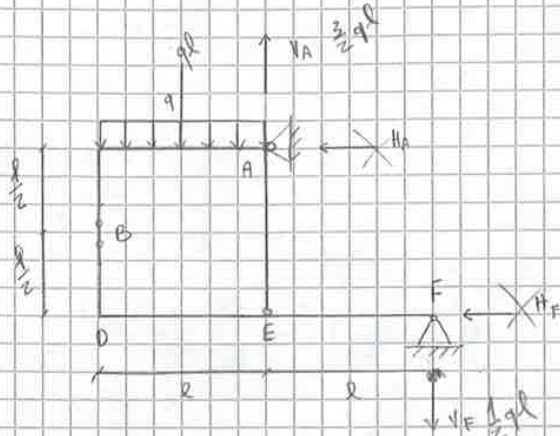


$$\frac{\sqrt{2}}{4} \cdot \frac{-3(\sqrt{2}-1)EI\chi t}{l} = \frac{-3(\sqrt{2}-1)EI\chi t}{4l}$$

CORREZIONE  
TEMA D'ESAME 18/7/2013

ES. 1

1.1)

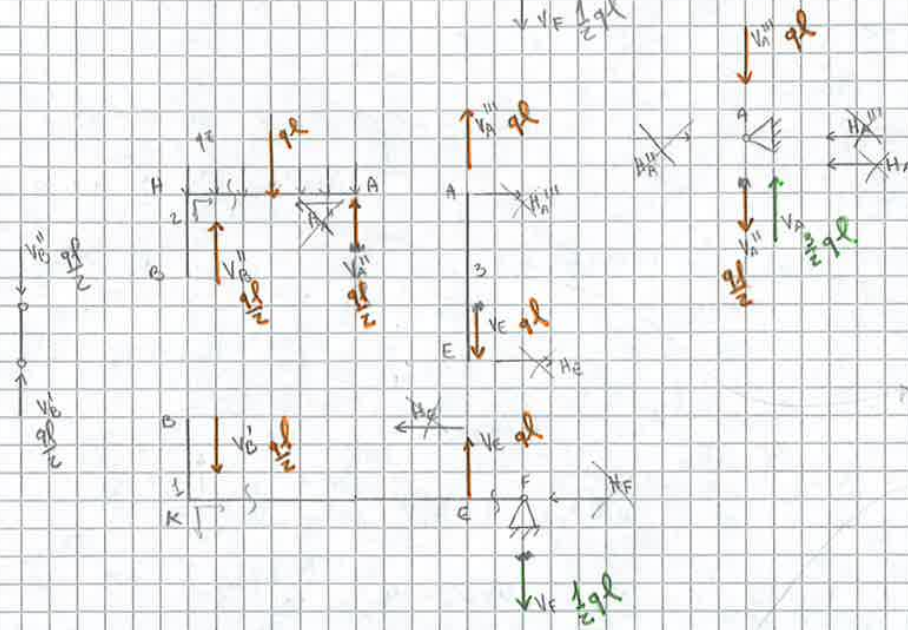


reazioni vincolari:

$$\rightarrow -H_A - H_F = 0$$

$$\uparrow -ql + V_A + V_F = 0$$

$$\curvearrowright M(F) = ql \cdot \frac{3}{2}l - V_A \cdot l + H_A \cdot l$$



corpo 2:

$$\rightarrow -H_A'' = 0 \rightarrow H_A'' = 0$$

$$\uparrow V_B'' - V_A'' - ql = 0 \rightarrow V_A'' = -\frac{ql}{2}$$

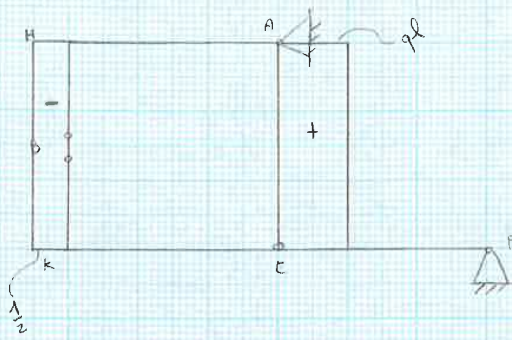
$$\curvearrowright M(A) = -V_B'' \cdot l + ql \cdot \frac{l}{2} = 0$$

$$-V_B'' \cdot l = -\frac{ql^2}{2} \rightarrow V_B'' = \frac{ql}{2}$$

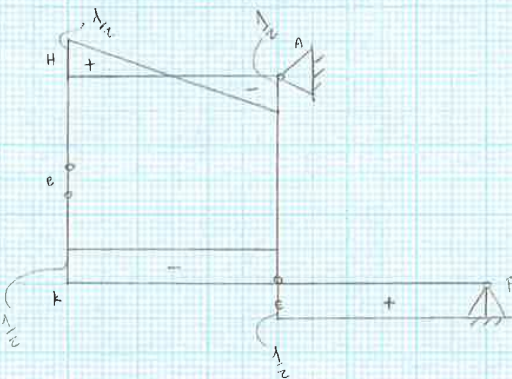
$$\approx H_A = 0 \quad M(F) = \frac{3}{2}ql^2 - V_A \cdot l + H_A \cdot l = 0 \rightarrow H_A = \frac{3}{2}ql$$

equilibrio nodo A:

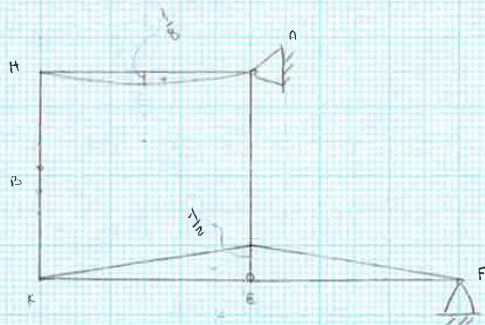
$$\uparrow -\frac{ql}{2} + \frac{3}{2}ql - V_A''' = 0 \rightarrow V_A''' = ql$$



$$\frac{N}{qd}$$

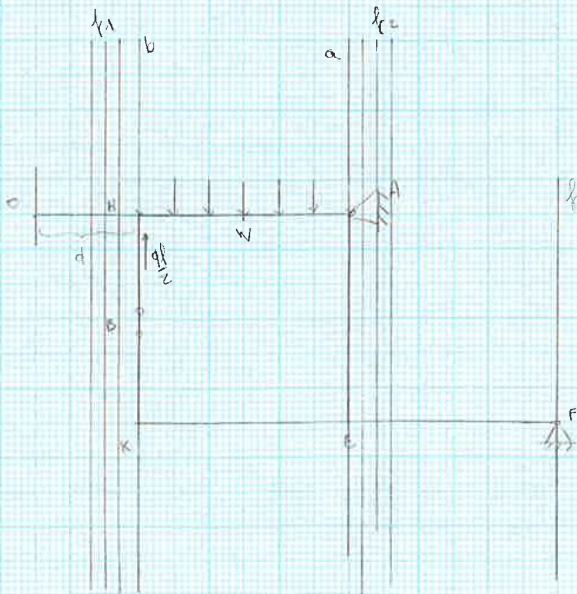


$$\frac{T}{qd}$$



$$\frac{M}{qd^2}$$

1.2)



$$\sum M(z) = qd \cdot d - qz \left( \frac{z}{2} + d \right) = 0$$

$$\frac{ld}{z} - zd - \frac{z^2}{2} = 0$$

$$ld - z^2d - \frac{z^3}{2} = 0$$

$$d(l - 2z^2) - \frac{z^3}{2} = 0$$

$$d(z) = \frac{z^3}{(l - 2z^2)}$$

$$z < \frac{l}{\sqrt{2}} \quad d(z) > 0 \rightarrow \text{sx di H}$$

$$z > \frac{l}{\sqrt{2}} \quad d(z) < 0 \rightarrow \text{dx di H}$$

$$z \rightarrow \frac{l}{\sqrt{2}} \quad d(z) = \left( \frac{l}{\sqrt{2}} \right)^2 = +\infty$$

$$z \rightarrow \frac{l}{\sqrt{2}} \quad d(z) = \left( \frac{l}{\sqrt{2}} \right)^2 = -\infty$$

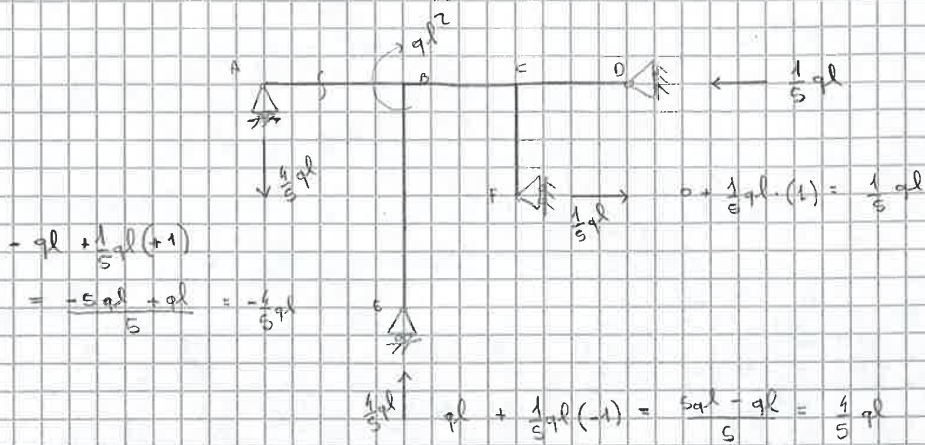
tratto	cdp
FE	retta f
EK	retta a
BH	retta b
HW	fascio f1
WA	fascio f2
AC	retta e

2 fasci estremi per HW → fascio a sx di H  
 ed i vincoli WA → fascio a dx di A



reazioni vincolari:  $R = R_0 + R_1 x_1$

$x_1 = \frac{1}{5} ql$



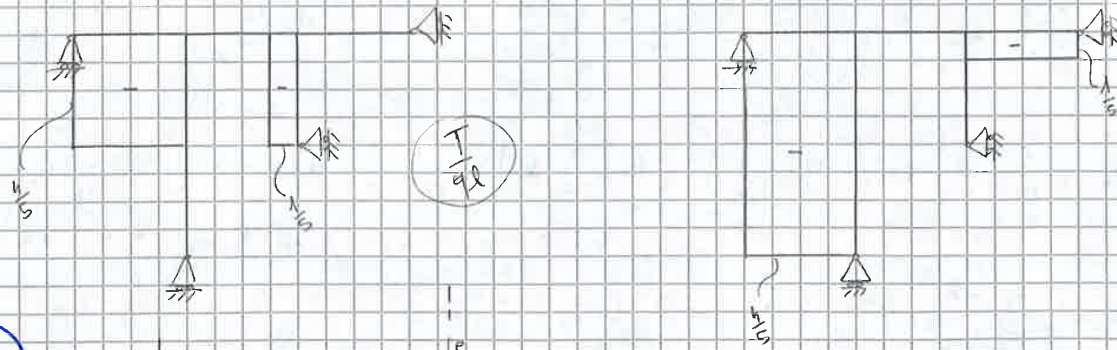
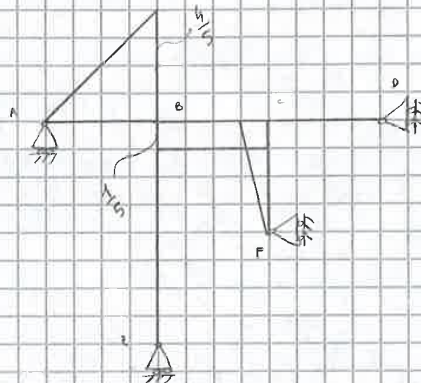
$M = M_0 + M_1 x_1$

$\overline{AB} \quad M = -\frac{4}{5} ql \cdot z$

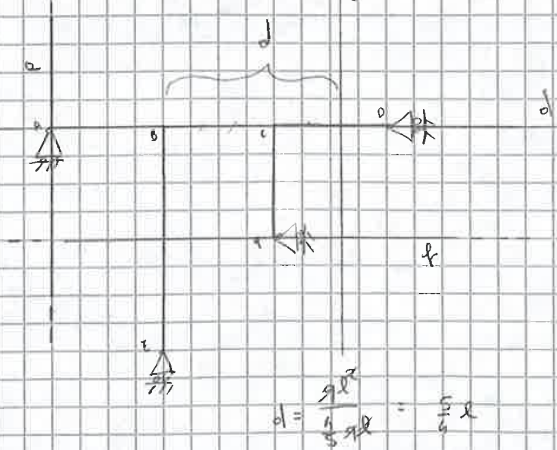
$M(0) = M_A = 0$

$M(l) = M_B = -\frac{4}{5} ql^2$

$\overline{BC} \quad M = 0 + l \cdot \frac{1}{5} ql = \frac{ql^2}{5}$



2.2)



tratto	cdp
AB	retta a
BC	retta b
CD	retta c

$d = \frac{ql^2}{5 ql} = \frac{1}{5} l$

$$\eta^{(2)} = H_E = \int_S \frac{M_1^{(1)} \cdot M_1^{(2)}}{EI} dz$$

$$\begin{aligned} \frac{1}{EI} \int_A^B M_1 \cdot M_2 dz &= \frac{l}{6} \left[ 0 \cdot 0 + 4 \cdot \left(\frac{l}{3}\right) \cdot \left(-\frac{2}{5} ql^2\right) + (l) \cdot \left(-\frac{4}{5} ql^2\right) \right] \\ &= \frac{l}{6} \left[ -\frac{8}{5} ql^3 - \frac{4}{5} ql^3 \right] = \frac{l}{6} \cdot \left(-\frac{12}{5} ql^3\right) = -\frac{2}{15} ql^4 \cdot \frac{1}{EI} \end{aligned}$$

$$\begin{aligned} \frac{1}{EI} \int_B^C M_1 \cdot M_2 dz &= \frac{l}{6} \left[ l \cdot \left(\frac{1}{5} ql^2\right) + 4 \cdot (l) \cdot \left(\frac{1}{5} ql^2\right) + l \cdot \left(\frac{1}{5} ql^2\right) \right] \\ &= \frac{l}{6} \left(\frac{6}{5} ql^3\right) = \frac{1}{5} ql^4 \cdot \frac{1}{EI} \end{aligned}$$

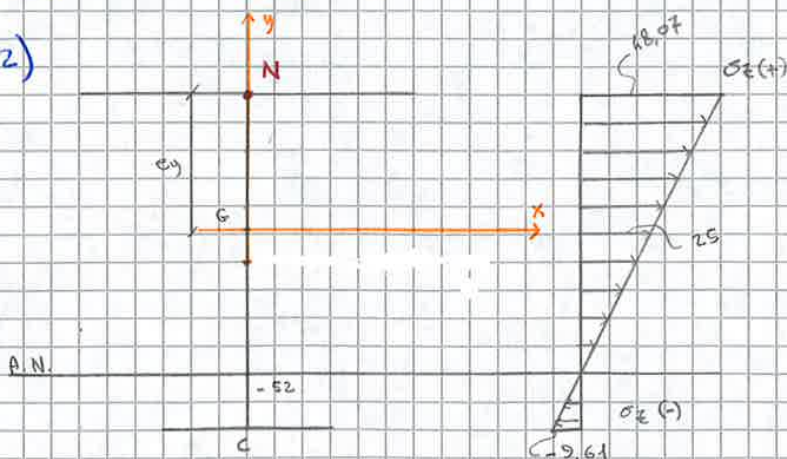
$$\begin{aligned} \frac{1}{EI} \int_C^D M_1 \cdot M_2 dz &= \frac{l}{6} \left[ 0 \cdot 0 + 4 \cdot \left(\frac{l}{3}\right) \cdot \left(-\frac{2}{5} ql^2\right) + l \cdot \left(-\frac{4}{5} ql^2\right) \right] \\ &= \frac{l}{6} \left[ -\frac{8}{5} ql^3 - \frac{4}{5} ql^3 \right] = \frac{l}{6} \cdot \left(-\frac{12}{5} ql^3\right) = -\frac{2}{15} ql^4 \cdot \frac{1}{EI} \end{aligned}$$

$$H_E = \left(-\frac{2}{15} + \frac{1}{5} - \frac{2}{15}\right) \frac{ql^4}{EI} = \left(\frac{-4 + 3 - 2}{15}\right) \frac{ql^4}{EI} = -\frac{3}{15} \frac{ql^4}{EI}$$

ES. 3

3.1) ok (vedi compito)

3.2)



$$N = 22,5 \text{ kN} = 22,5 \cdot 10^3 \text{ N}$$

$$\sigma_x = \frac{N}{A} + \frac{M_x \cdot y}{I_x} - \frac{M_y \cdot x}{I_y}$$

$$M_x = N \cdot e_y = N \cdot (120 - 72) = N \cdot 48$$

$$M_y = -N \cdot e_x = 0$$

$$\text{A.N. } 1 + \frac{e_y}{\rho_x^2} \cdot y + \frac{e_x}{\rho_y^2} \cdot x = 0$$

$$\rho_x^2 = \frac{I_x}{A} = \frac{2 \cdot 246 \cdot 400}{900} = 2496$$

$$1 + \frac{48}{2496} \cdot y = 0 \rightarrow 1 + 0,0192 y = 0 \rightarrow y = -\frac{1}{0,0192} = -52,1$$

$$S_x(72) = -216(72) + \frac{3}{2}(72)^2 - 12960 = -15552 + 7776 - 12960 = -20736$$

$$S_x(0) = -12960$$

$$\gamma_{zx}(S_1) = \frac{T_y \cdot (144 \cdot S_1)}{3 \cdot (2246400)} = \frac{15 \cdot 10^3 \cdot (144) \cdot S_1}{3 \cdot (2246400)}$$

$$1) \gamma_{zx}(0) = 0$$

$$2) \gamma_{zx}(60) = \frac{15 \cdot 10^3 \cdot 8640}{3 \cdot (2246400)} = 19,23$$

$$\gamma_{zy}(S_2) = \frac{15 \cdot 10^3 \cdot (144 S_2 - \frac{3}{2} S_2^2 + 17280)}{3 \cdot (2246400)}$$

$$1) \gamma_{zy}(0) = \frac{15 \cdot 10^3 \cdot 17280}{3 \cdot (2246400)} = 38,46$$

$$2) \gamma_{zy}(48) = \frac{15 \cdot 10^3 \cdot 20736}{3 \cdot (2246400)} = 46,15$$

$$\gamma_{zy}(S_1) = \frac{15 \cdot 10^3 \cdot (-216 S_1)}{3 \cdot (2246400)}$$

$$1) \gamma_{zy}(0) = 0$$

$$2) \gamma_{zy}(30) = \frac{15 \cdot 10^3 \cdot (-6480)}{3 \cdot (2246400)} = 14,92$$

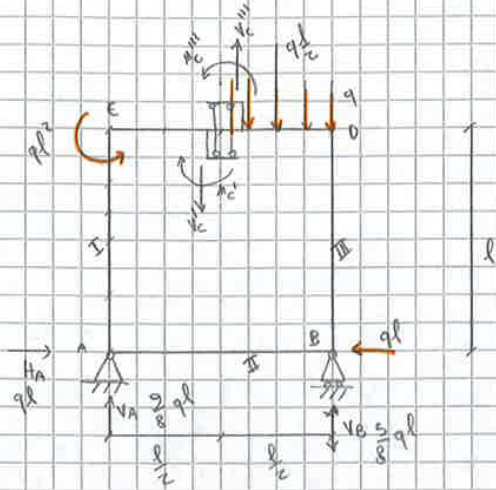
$$\gamma_{zy}(72) = \frac{15 \cdot 10^3 \cdot (-20736)}{3 \cdot 2246400} = 46,15$$

$$\gamma_{zy}(0) = \frac{15 \cdot 10^3 \cdot (-12960)}{3 \cdot 2246400} = 28,84$$

TEMA D'ESAME 28/6/2011

COMPITO I

ES. 1)



$$g = 3 \cdot 3 = 9$$

$$V = 3 + 2 + 2 + 2 = 9$$

Isostatica

reazioni vincolari:  $\uparrow \leftarrow$

$$\rightarrow H_A - ql = 0 \rightarrow H_A = ql$$

$$\uparrow V_A + V_B - ql = 0$$

$$V_B = \frac{4}{8}ql - \frac{3}{8}ql = -\frac{5}{8}ql$$

$$\sum M(B) = -V_A \cdot l + ql^2 + ql \cdot \frac{l}{4} = 0$$

$$-V_A \cdot l + \frac{8}{8}ql^2 + \frac{ql^2}{8} = 0$$

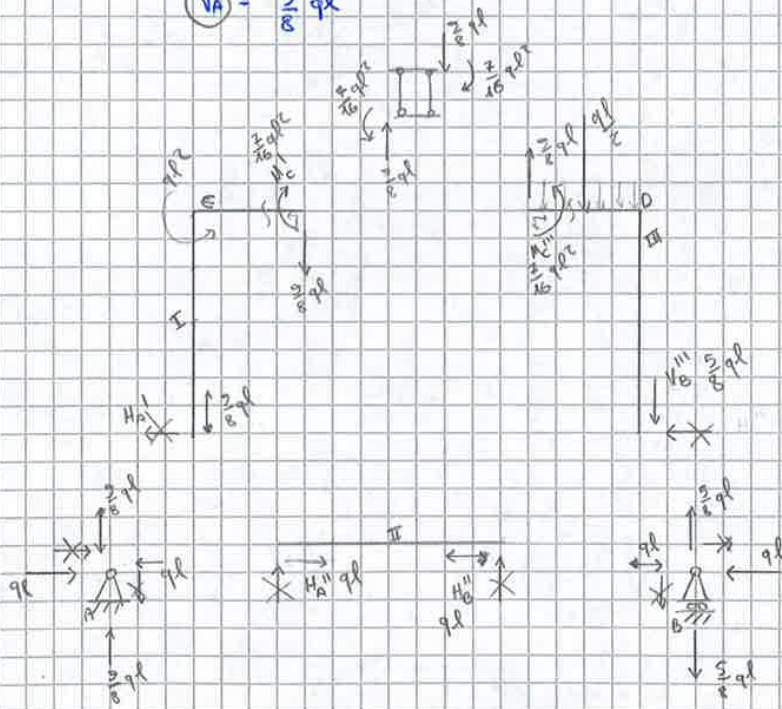
$$V_A = \frac{9}{8}ql$$

corpo I:

$$\sum M(c) = -\frac{7}{16}ql^2 + ql^2 - \frac{3}{8}ql \cdot \frac{l}{2} + H_A \cdot l$$

$$= -\frac{7}{16}ql^2 + ql^2 - \frac{3}{16}ql^2 + H_A \cdot l = 0$$

$$H_A = \frac{(-7 + 16 - 3)ql}{16} = 0$$



corpo I:

$$\sum M(A) = ql^2 - M_c - \frac{3}{8}ql \cdot \frac{l}{2} = 0$$

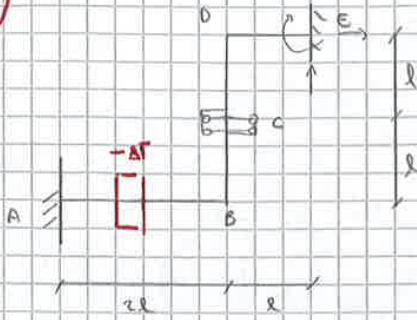
$$M_c = ql^2 - \frac{3}{16}ql^2 = \frac{7}{16}ql^2$$

corpo III:

$$\uparrow \frac{3}{8}ql - ql - V_B''' = 0$$

$$V_B''' = \frac{3-4}{8}ql = -\frac{1}{8}ql$$

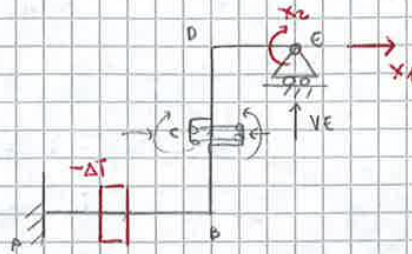
ES.2)



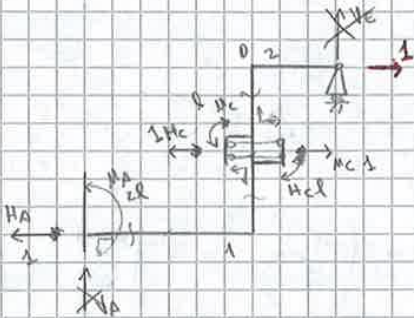
2-volte iprc

$$g = 2 \cdot 3 = 6$$

$$V = 3 + 3 + 2 = 8$$



sistema (Q1):



reazioni vincolari:  $\begin{matrix} \uparrow \\ \rightarrow \end{matrix}$

$$\rightarrow H_A + 1 = 0 \rightarrow H_A = -1$$

$$\uparrow V_A + V_E = 0$$

$$\circlearrowleft M(E) = -V_A \cdot 3l - 1 \cdot 2l + M_A = 0$$

corpo 2:  $\circlearrowleft M(E) = -1 \cdot l - M_C = 0$

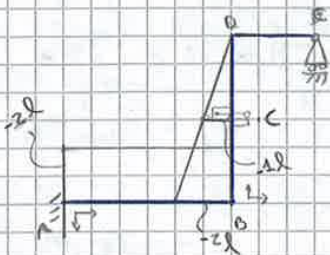
$$M_C = -l$$

corpo I:  $\circlearrowleft M(A) = M_A - l - 1 \cdot l = 0$

$$M_A = 2l$$

$$-V_A \cdot 3l - 2l + 2l = 0$$

$$V_A = 0$$



$M_1$

$\overline{CB}$   $M = l + 1 \cdot z$

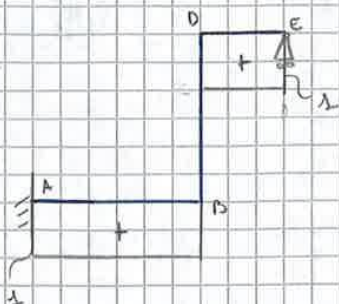
$$M(0) = M_C = l$$

$$M(l) = M_B = 2l$$

$\overline{CO}$   $M = -l + 1 \cdot z$

$$M(0) = M_C = -l$$

$$M(l) = M_D = 0$$



$N_1$



$$\int_A^B M_1 M_2 dz = \frac{2l}{6} (1 \cdot (-1) + 4(1)(-1) + (-1)(1)) = \frac{2l}{6} (-1 - 4 - 1) = -2l$$

$$\int_A^B M_1 M_2 dz = \frac{2l}{6} ((-2)(-1) + 4(-2)(-1) + (-2)(-1)) = \frac{2l}{6} (2 + 8 + 2) = 4l^2$$

$$\int_B^C M_1 M_2 dz = \frac{2l}{6} ((-2)(-1) + 4(-1)(-1)) = \frac{2l}{6} (2 + 4) = 2l^3$$

$$\int_A^B \frac{M_1 M_2 dz}{EI} = \frac{6l^2}{EI}$$

$$\int_A^B M_2^2 dz = \frac{2l}{6} ((-1)^2 + 4(-1)^2 + (-1)^2) = 2l$$

$$\int_B^C M_2^2 dz = \frac{2l}{6} ( \dots ) = 2l$$

$$\int_C^D M_2^2 dz = \frac{l}{6} ((-1)^2 + 4(-1)^2 + (-1)^2) = l$$

$$\int_0^l \frac{M_2^2 dz}{EI} = \frac{5l}{EI}$$

$$\begin{cases} 2l Et + \frac{32}{3} \frac{l^3}{EI} x_1 + 6 \frac{l^2}{EI} x_2 = 0 \\ 6 \frac{l^2}{EI} x_1 + 5 \frac{l}{EI} x_2 = 0 \end{cases}$$

$$x_1 = -5 \frac{l}{EI} x_2 \cdot \frac{EI}{l^2 6} = -\frac{5}{6l} x_2$$

$$2l Et + \frac{32}{3} \frac{l^3}{EI} \left( -\frac{5}{6} \frac{x_2}{l} \right) + 6 \frac{l^2}{EI} x_2 = 0$$

$$x_1 = -\frac{5}{26} \cdot \frac{26}{13} \frac{6l EI}{l}$$

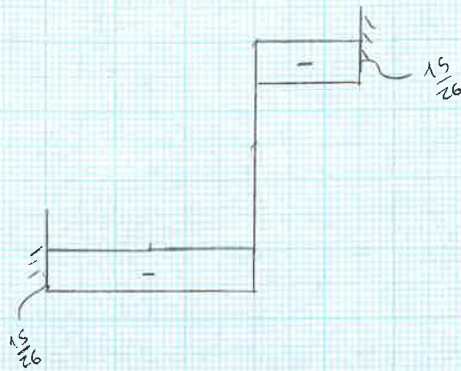
$$= -\frac{15}{26} \frac{6l EI}{l}$$

$$2l Et - \frac{160}{18} \frac{l^2}{EI} x_2 + 6 \frac{l^2}{EI} x_2 = 0$$

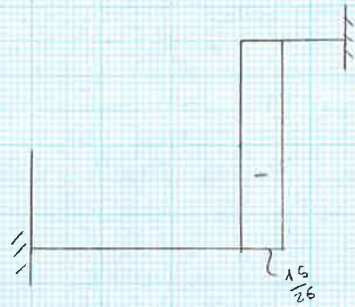
$$\frac{-160 l^2 x_2 + 108 l^2 x_2}{18 EI} = -2l Et$$

$$x_2 = \frac{9}{13} \frac{6l EI}{l}$$

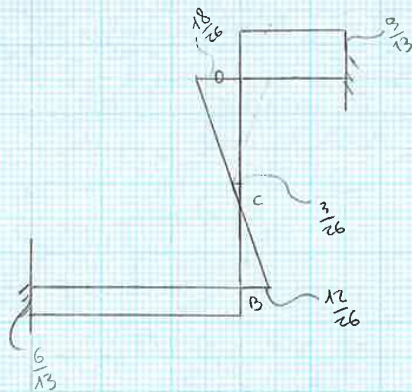
$$-\frac{52}{18} \frac{l^2 x_2}{EI} = -2l^2 Et \rightarrow x_2 = 2 \cdot \frac{18}{52} \cdot l Et \cdot \frac{EI}{l}$$



$$\frac{N}{6EI} \cdot l$$



$$\frac{T}{6EI} \cdot l$$



$$\overline{BC} \quad M = \frac{15}{26} \frac{EI}{l} \cdot l - \frac{3}{26} \frac{EI}{l} \cdot l$$

$$\overline{CD} \quad M = -\frac{15}{26} \frac{EI}{l} \cdot l - \frac{3}{26} \frac{EI}{l} \cdot l$$

grafici ok  
ma ricalcolati



$$\theta_0 = \frac{1}{2} \arctan \frac{I_{xy}}{\frac{I_y}{2} - \frac{I_x}{2}} = \frac{2 \cdot 86,49}{(332,94 - 480,30)} = -29,78^\circ$$

$$I_{\xi} = \frac{480,30 + 332,94}{2} \pm \frac{1}{2} \sqrt{(480,30 - 332,94)^2 + 4(86,49)^2}$$

$$= 406,62 \pm \frac{1}{2} \sqrt{113,62}$$

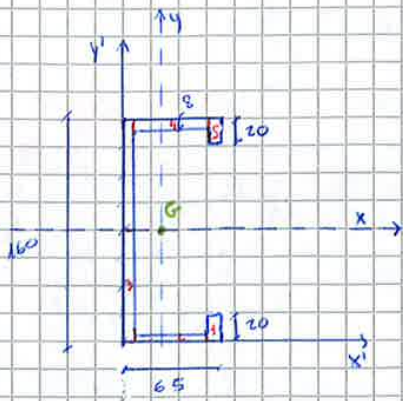
$$\rightarrow I_{\xi} = 520,23$$

$$\rightarrow I_{\eta} = 293$$

$$I_x > I_y$$

$$I_{\xi} > I_{\eta}$$

ES. 2



l'asse x è di simmetria perciò il baricentro G sta su di esso:

$y_G \text{ noto} = \frac{160}{2} \Rightarrow$  distanza da asse  $x'$

$x_G = \frac{S_{y'}}{A} \Rightarrow$  distanza da asse  $y'$

asse di simmetria (simmetria assiale retta)

scempesta la figura in 5 rettangoli si ha:

$S_{y1}' = A \cdot x_{G1} = 20 \cdot 8 \cdot (65 - \frac{8}{2}) = 9760$

$S_{y2}' = A \cdot x_{G2} = (65 - 8 \cdot 2) \cdot 8 \cdot (\frac{65}{2}) = 12740$

$S_{y3}' = A \cdot x_{G3} = (160 \cdot 8) \cdot \frac{8}{2} = 5120$

$S_{y' tot} = 5120 + 2 \cdot [9760 + 12740] = 50120 \text{ mm}^3$

$A_{tot} = 2 \cdot (20 \cdot 8 + (65 - 16) \cdot 8) + 160 \cdot 8 = 1280 + 2104 = 2384 \text{ mm}^2$

$x_G = \frac{S_{y'}}{A} = \frac{50120}{2384} = 21 \text{ mm}$

$G(21; 80) \rightarrow$  coordinate rispetto ad  $x'y'$

Momenti di inerzia rispetto ad  $x'y'$  (assi baricentrici e principali):

$I_{xG}^{(1)} = I_{xG1} + A \cdot (y_G - y_{G1})^2 = \frac{20 \cdot 8^3}{12} + (20 \cdot 8) \cdot ((\frac{10}{2}) - 80)^2 = 789333,3$

$I_{xG}^{(2)} = I_{xG2} + A \cdot (y_G - y_{G2})^2 = \frac{8^3 \cdot 19}{12} + (19 \cdot 8) \cdot (80 - \frac{65}{2})^2 = 226282,6$

$I_{xG}^{(3)} = I_{xG3} + A \cdot (y_G - y_{G3})^2 = \frac{160^3 \cdot 8}{12} + (160 \cdot 8) \cdot (80 - 80)^2 = 2730666,6$

$I_{xG}^{tot} = 2 \cdot (I_{xG}^{(1)} + I_{xG}^{(2)}) + I_{xG}^{(3)} = 8841898,4 \text{ mm}^4$

potrebbe anche calcolarsi come differenza tra il momento di inerzia del rettangolo circoscritto e la somma tra il momento del rettangolo interno e del rettangolo di dimensioni  $8 \times 120$ :

$I_x = \frac{65 \cdot 160^3}{12} - (\frac{49 \cdot 144^3}{12} + \frac{8 \cdot 120^3}{12}) = 8841898 \text{ mm}^4$

$$\underline{I_{x_G} = 691.934,08}$$

$$I_{y_G^{(1)}} = I_{y_{G1}} + A(x_G - x_{G1})^2 = \frac{45^3 \cdot 20}{12} + (45 \cdot 20) \cdot (16,33 - 22,5)^2 = 186.137,01$$

$$I_{y_G^{(2)}} = I_{y_{G2}} + A(x_G - x_{G2})^2 = \frac{15^3 \cdot 50}{12} + (50 \cdot 15) \cdot (16,33 - 7,5)^2 = 72.539,17$$

$$I_{y_G^{(3)}} = I_{y_{G3}} + A(x_G - x_{G3})^2 = \frac{20^3 \cdot 20}{36} + \left(\frac{20 \cdot 20}{2}\right) \cdot (16,33 - 21,67)^2 = 10.147,56$$

$$\underline{I_{y_{G_{TOT}}} = 268.823,74 \text{ mm}^4}$$

$$I_{x_G y_G^{(1)}} = \cancel{I_{x_{G1} y_{G1}}} + A \cdot (y_G - y_{G1})(x_G - x_{G1}) = + (20 \cdot 45) (25,99 - 10) (16,33 - 22,5) = -88.792,47$$

$$I_{x_G y_G^{(2)}} = \cancel{I_{x_{G2} y_{G2}}} + A \cdot (y_G - y_{G2})(x_G - x_{G2}) = + \left(\frac{50 \cdot 15}{2}\right) \cdot (25,99 - 10) \cdot (16,33 - 7,5) = 125.893,72$$

$$I_{x_G y_G^{(3)}} = \cancel{I_{x_{G3} y_{G3}}} + A \cdot (y_G - y_{G3})(x_G - x_{G3}) = + \left(\frac{20^2 \cdot 20}{72}\right) + \left(\frac{20 \cdot 20}{2}\right) (25,99 - 26,66) (16,33 - 21,66) = -1.508,0$$

$$I_{x_G y_G} = -216.194,2 \text{ mm}^4$$

$$\theta_0 = \frac{1}{2} \arctan \left( \frac{2 I_{x_G y_G}}{I_{yy} - I_{xx}} \right) = \frac{1}{2} \arctan \left( \frac{2 \cdot (-216.194,2)}{268.823,74 - 691.934,08} \right) = \frac{1}{2} \arctan(1,0219) = 22,81^\circ$$

$$\underline{I_E = \frac{(I_x + I_y)}{2} + \frac{1}{2} \sqrt{(I_x - I_y)^2 + 4 I_{xy}^2}} = 782.852 \text{ mm}^4$$

$$\underline{I_H = \frac{(I_x + I_y)}{2} - \frac{1}{2} \sqrt{(I_x - I_y)^2 + 4 I_{xy}^2}} = 177.896 \text{ mm}^4$$

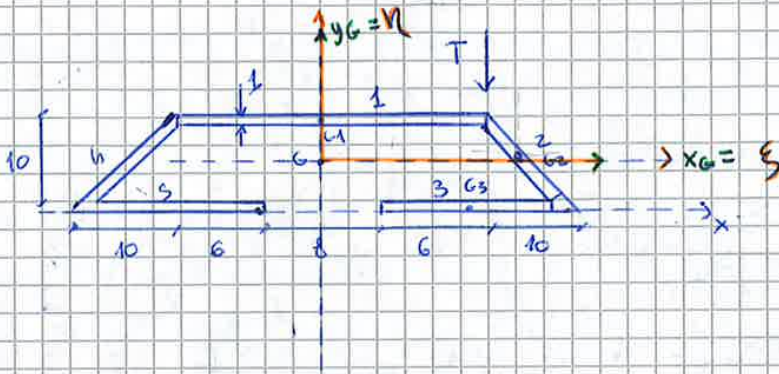
↳ assi baricentrici ≠ da assi principali

$$I_{\xi} = \left( \frac{194.667 + 72.000}{2} \right) + \frac{1}{2} \sqrt{(194.667 - 72.000)^2 + 4 \cdot (36.000)^2} = 204.000$$

$$I_{\eta} = 62.000$$

$$\theta_0 = \frac{1}{2} \arctan \left( \frac{2 \cdot 36.000}{72.000 - 194.667} \right) = -15,2^\circ$$

ES. 5 esame 26 luglio 2011



$$S_x^{(1)} = y_{G1} \cdot A_1 = 10 \cdot (20) = 200$$

$$S_x^{(2)} = y_{G2} \cdot A_2 = 5 \cdot (10) = 50$$

$$S_x^{(3)} = y_{G3} \cdot A_3 = 0 \cdot (16) = 0$$

$$S_{xTOT} = 270,71$$

$$A_{TOT} = 20 + 10 \cdot 5 + 16 = 50,14$$

$$y_G = \frac{S_{xTOT}}{A_{TOT}} = \frac{270,71}{50,14} = 5,39 \quad 4,25 \quad G = \left( 0; \begin{matrix} 4,25 \\ 5,39 \end{matrix} \right)$$

$$I_{xG}^{(1)} = I_{xG1} + A(y_G - y_{G1})^2 = 0 + (20) \cdot (5,39 - 10)^2 = 125,00 \quad 161,25$$

$$I_{xG}^{(2)} = I_{xG2} + A(y_G - y_{G2})^2 = \frac{1 \cdot (10)^3}{12} \sin^2 45^\circ + (10) \cdot (5,39 - 5)^2 = 123,78 \quad 125,80$$

$$I_{xG}^{(3)} = I_{xG3} + A(y_G - y_{G3})^2 = 0 + (16 \cdot 1) \cdot (5,39 - 0)^2 = 469,83 \quad 289$$

$$I_{xTOT} = I_{xG}^{(1)} + 2(I_{xG}^{(2)} + I_{xG}^{(3)}) = 1.490,85 = I_{\xi}$$

$$I_{yG}^{(1)} = I_{yG1} + A(x_G - x_{G1})^2 = \frac{1 \cdot 20^3}{12} + (20) \cdot (0)^2 = 666,66$$

$$I_{yG}^{(2)} = I_{yG2} + A(x_G - x_{G2})^2 = \frac{(10)^3}{12} \cdot 1 \cos^2 45^\circ + (10) \cdot (0 - 15)^2 = 3.299,83$$

$$I_{yG}^{(3)} = I_{yG3} + A(x_G - x_{G3})^2 = \frac{16^3 \cdot 1}{12} + (16) \cdot (0 - 12)^2 = 2.645,33$$

$$I_{yTOT} = 12.556,92 = I_{\eta}$$

$I_{xG-yG} = 0$  x simmetrica  
 (gli assi principali sono anche  
 assi) orizzontali e verticali  $\Rightarrow$  assi centrali

$$I_{y_G}^{(1)} = I_{y_{G1}} + A(x_G - x_{G1})^2 = \frac{100 \cdot 5}{12} = 416'666,66$$

$$I_{y_G}^{(2)} = I_{y_{G2}} + A(x_G - x_{G2})^2 = 0$$

$$I_{y_G}^{(3)} = I_{y_{G3}} + A(x_G - x_{G3})^2 = \frac{50 \cdot 5}{12} = 52'083,33$$

$$I_{y_G}^{(4)} = I_{y_{G4}} + A(x_G - x_{G4})^2 = \frac{47 \cdot 5}{12} = 0$$

$$I_{y_{G_{TOT}}} = 468'749,99$$

$$I_{x_G y_G}^{(1)} = I_{x_{G1} y_{G1}} + A(x_G - x_{G1})(y_G - y_{G1}) = 0 + 0 = 0$$

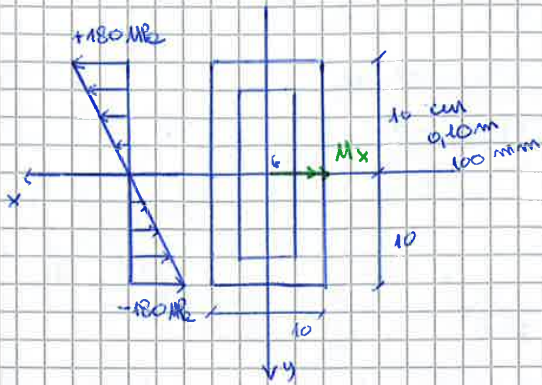
$$I_{x_G y_G}^{(2)} = I_{x_{G2} y_{G2}} + A(x_G - x_{G2})(y_G - y_{G2}) = 0 + 0 = 0$$

$$I_{x_G y_G}^{(3)} = 0$$

$$I_{x_G y_G}^{(4)} = 0$$

$$I_{x_G y_G} = 0$$

gli assi baracentrici  
sono anche assi  
principali  
(assi centroidali)



$$\sigma_z = \frac{M_x}{I_x} \cdot y$$

$$I_x = 3333,33 \text{ cm}^4$$

$$3333,33 \cdot 10^4 \text{ mm}^4$$

$$M_x = -60 \text{ kN} \cdot \text{m}$$

$$-60 \cdot 10^3 \text{ kN} \cdot \text{mm}$$

$$\sigma_z = \frac{-60 \cdot 10^3}{3333,33 \cdot 10^4} \cdot y = -0,0018 \cdot y \frac{\text{kN}}{\text{mm}^2}$$

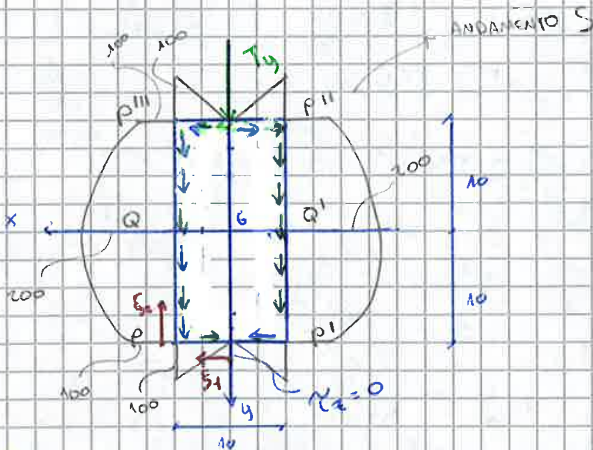
$$= -1,8 \cdot y \frac{\text{kN}}{\text{mm}^2}$$

tensioni max in corrispondenza del lato inferiore e superiore della trave.

A.N. = asse x  $\rightarrow y=0$   $\sigma_z=0$

$$\sigma_{\text{max}} = \sigma_z(-100) = -1,8 \cdot (-100) = 180 \frac{\text{N}}{\text{mm}^2} \text{ (MPa)}$$

$$\sigma_{\text{max}} = \sigma_z(100) = -1,8 \cdot (100) = -180 \frac{\text{N}}{\text{mm}^2} \text{ (MPa)}$$



$$\tau_z = \frac{T_y \cdot S_x^{(A)}}{2 I_x \cdot b}$$

$\rightarrow$  si può usare formula WSKY solo perché la sezione è simmetrica rispetto ad asse y

coordinate  $\xi_1$   $\xi_2$

$\rightarrow$  si misura da punto in cui  $\tau=0$

pp I

$$S_x^{A'}(\xi_1) = 2 \cdot (1 \cdot \xi_1 \cdot 10) = 20 \xi_1 \text{ cm}^3$$

$$S_x^A(5) = 2 \cdot 5 \cdot 10 = 100 \text{ cm}^3$$

pp III :

$$S_x^{A'}(\xi_2) = 2 \cdot \left( (1 \cdot \xi_2 \cdot (10 - \xi_2/2)) + 5 \cdot 10 \right)$$

$$= 20 \xi_2 - \xi_2^2 + 100 \quad \rightarrow \text{parabolico}$$

momento statico max

$$\frac{d S_x}{d \xi_2} = 0 \quad 20 - 2 \xi_2 = 0 \quad \rightarrow \xi_2 = 10$$

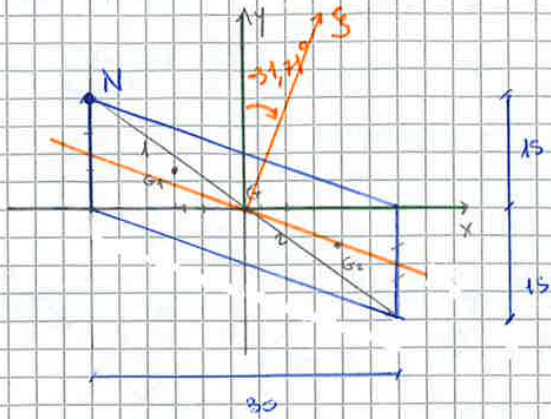
in corrispondenza delle 2 corde orizzontali

$$S_x^{A'}(10) = 20 \cdot 10 - 10^2 + 100 = 200 \quad \rightarrow S_{x \text{ max}}^{A'}$$

$$S_x^{A'}(0) = 100$$



ES. 8 esame 26 GIUGNO 2012 ES. 3



$$A_{1,2} = \frac{30 \cdot 15}{2} = 225$$

$$A_{TOT} = 225 \cdot 2 = 450$$

$$S_x^{(1)} = y_{G1} \cdot A_1 = 5 \cdot \frac{30 \cdot 15}{2} = 1125$$

$$S_x^{(2)} = y_{G2} \cdot A_2 = (-5) \cdot \frac{30 \cdot 15}{2} = -1125$$

sezione a simmetria piana (baricentro = centro geometrico)

1)

$$I_{x_G}^{(1)} = I_{x_{G1}} + A \cdot y_G^2 = I_{x_{G1}} + A(y_G - y_{G1})^2 = \frac{15^3 \cdot 30}{36} + \frac{30 \cdot 15}{2} (0 - 5)^2 = 8437,5$$

$$I_{x_G}^{(2)} = I_{x_{G2}} + A \cdot y_G^2 = I_{x_{G2}} + A(y_G - y_{G2})^2 = \frac{15^3 \cdot 30}{36} + \frac{30 \cdot 15}{2} (0 + 5)^2 = 8437,5$$

$$I_{x_G-TOT} = 16875 \text{ mm}^4$$

$$I_{y_G}^{(1)} = I_{y_{G1}} + A \cdot (x_G - x_{G1})^2 = \frac{15 \cdot 30^3}{36} + \frac{30 \cdot 15}{2} (0 + 5)^2 = 16875$$

$$I_{y_G}^{(2)} = I_{y_{G2}} + A \cdot (x_G - x_{G2})^2 = \frac{15 \cdot 30^3}{36} + \frac{30 \cdot 15}{2} (0 - 5)^2 = 16875$$

$$I_{y_G-TOT} = 33750$$

$$I_{x_G y_G}^{(1)} = I_{x_G y_G1} + A \cdot (y_G - y_{G1})(x_G - x_{G1}) = -\frac{30^2 \cdot 15^2}{72} + 225 \cdot (0 - 5) \cdot (0 + 5) = -2812,5 - 5625 = -8437,5$$

$$I_{x_G y_G}^{(2)} = I_{x_G y_G2} + A \cdot (y_G - y_{G2})(x_G - x_{G2}) = -\frac{30^2 \cdot 15^2}{72} + 225 \cdot (0 + 5) \cdot (0 - 5) = -8437,5$$

$$I_{x_G y_G-TOT} = -16875$$

$$I_S = \frac{(I_x + I_y)}{2} - \frac{1}{2} \sqrt{(I_x - I_y)^2 + 4 \cdot I_{xy}^2} = \frac{(16875 + 33750)}{2} - \frac{1}{2} \sqrt{(16875 - 33750)^2 + 4 \cdot (-16875)^2}$$

$$= 25312,5 - 18866,82 = 6445,68$$

$$I_{\bar{y}} = \frac{(I_x + I_y)}{2} + \frac{1}{2} \sqrt{(I_x - I_y)^2 + 4 \cdot I_{xy}^2} = 25312,5 + 18866,82 = 44179,32$$

tensione max nei punti + distanti da A.N. : N e K

$$\sigma_z = \frac{N}{A} + \frac{M_x}{I_{yy}} \cdot y - \frac{M_y}{I_{xx}} \cdot x$$

$$M_x = N \cdot e_y$$

$$M_y = -N \cdot e_x$$

$$N \begin{pmatrix} e_x = 20,64 \\ e_y = 4,88 \end{pmatrix}$$

$$K \begin{pmatrix} e_x = 20,64 \\ e_y = 4,88 \end{pmatrix}$$

$$K \begin{pmatrix} M_x = -20,64 \\ M_y = -4,88 \end{pmatrix}$$

K)

$$\sigma_z = \frac{N}{450} + \frac{N \cdot 4,88}{6445,68} \cdot (-20,64) - \frac{N \cdot 20,64}{44179,32} \cdot (-4,88)$$

$$I_y = 44179,32$$

$$I_x = 6445,68$$

$$A = 450$$

$$\sigma_z = N \left( \frac{1}{450} + \frac{23,76428}{6445,68} - \frac{100,7033}{44179,32} \right)$$

$$\sigma_z = N (-0,00396) \quad \rightarrow \quad N = \frac{\sigma_z}{-0,00396}$$

$$\sigma_{amm} = 255 \frac{N}{mm^2}$$

$$N = \frac{255}{-0,00396} = 64393,93$$

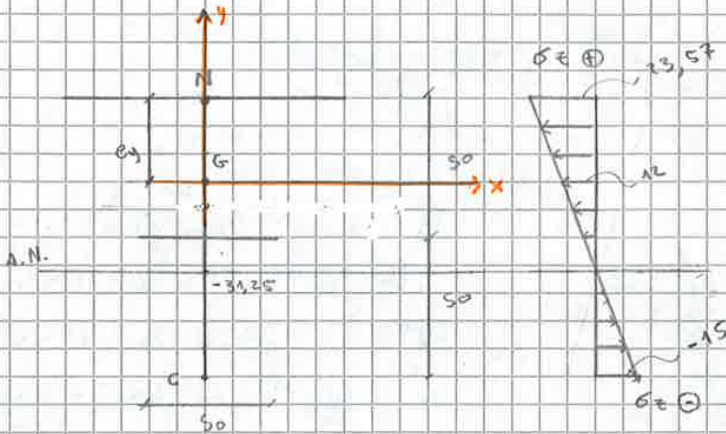
$$\begin{aligned}
 I_{xGyG}^{(1)} &= I_{xGyG_1} + A(y - y_{G_1})(x - x_{G_1}) = 0 \\
 I_{xGyG}^{(2)} &= I_{xGyG_2} + A(y - y_{G_2})(x - x_{G_2}) = 0 \\
 I_{xGyG}^{(3)} &= I_{xGyG_3} + A(y - y_{G_3})(x - x_{G_3}) = 0 \\
 I_{xGyG}^{(4)} &= I_{xGyG_4} + A(y - y_{G_4})(x - x_{G_4}) = 0
 \end{aligned}$$

tutti = 0

assi baricentrici sono anche assi principali (assi centrali)

STRESS NORMALE N:

$$N = 15 \text{ kN} = 15 \cdot 10^3 \text{ N}$$



$$\sigma_z = \frac{N}{A} + \frac{M_x}{I_x} y - \frac{M_y}{I_y} x$$

$$M_x = N \cdot e_y = N \cdot (100 - 70) = 30 \cdot N$$

$$M_y = -N \cdot e_x = 0$$

$$\text{A.N.} \quad 1 + \frac{e_y}{\rho_x^2} y + \frac{e_x}{\rho_y^2} x = 0$$

$$\rho_x^2 = \frac{I_x}{A} \quad \rho_y^2 = \frac{I_y}{A}$$

$$1 + \frac{30}{933,33} y = 0$$

$$1 + 0,032 y = 0$$

$$y = \frac{-1}{0,032} = -31,25$$

$$\rho_x^2 = \frac{1166666,66}{1250} = 933,33 \quad e_y = 30$$

$$\rho_y^2 = \frac{166749,99}{1250} = 133,39$$

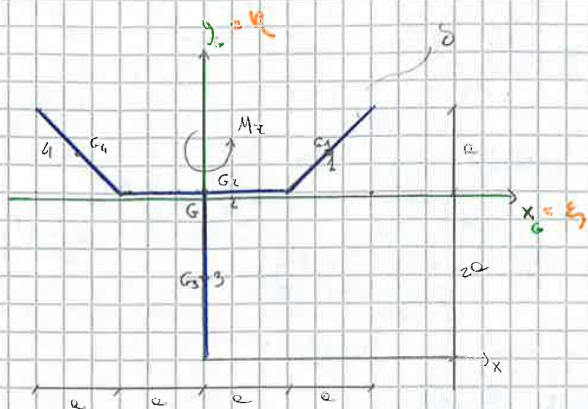
$$\begin{aligned}
 \sigma_z(y) = \sigma_z(N) = \sigma_z(30) &= \frac{N}{A} + \frac{N \cdot e_y}{I_x} \cdot 30 = \frac{15 \cdot 10^3}{1250} + \frac{15 \cdot 10^3 \cdot 30}{1166666,66} \cdot 30 \\
 &= 12 + 1,157 = 23,57 \frac{\text{N}}{\text{mm}^2} = \text{MPa}
 \end{aligned}$$

$$\begin{aligned}
 \sigma_z(y) = \sigma_z(C) = \sigma_z(-70) &= \frac{N}{A} + \frac{N \cdot e_y}{I_x} (-70) = 12 + \frac{15 \cdot 10^3 \cdot 30}{1166666,66} (-70) \\
 &= 12 - 27 = -15 \frac{\text{N}}{\text{mm}^2} = \text{MPa}
 \end{aligned}$$

$$\sigma_z(y) = \sigma_z(G) = \sigma_z(0) = 12$$

TEMA D'ESAME 20/9/1993

ES. 3)



$$A_1 = a\sqrt{2} \delta$$

$$A_2 = 2a \delta$$

$$A_3 = 2a \cdot \delta$$

$$A_4 = a\sqrt{2} \cdot \delta$$

$$A_{TOT} = \sum_{i=1}^4 A_i = 2(a\sqrt{2}\delta) + 2 \cdot (2a\delta) = 2\sqrt{2}a\delta + 4a\delta = 2a\delta(\sqrt{2} + 2)$$

$$S_x^{(1)} = y_{G1} \cdot A^{(1)} = \left(2a + \frac{a}{2}\right) \cdot (a\sqrt{2}\delta)$$

$$S_x^{(2)} = y_{G2} \cdot A^{(2)} = 2a \cdot (2a\delta)$$

$$S_x^{(3)} = y_{G3} \cdot A^{(3)} = a \cdot (2a\delta)$$

$$S_x^{(4)} = y_{G4} \cdot A^{(4)} = \left(2a + \frac{a}{2}\right) \cdot (a\sqrt{2}\delta)$$

$$S_{TOT} = \left(4a \cdot a\sqrt{2}\delta + a \cdot a\sqrt{2}\delta\right) + 4a^2\delta + 2a^2\delta = 4\sqrt{2}a^2\delta + \sqrt{2}a^2\delta + 6a^2\delta = 5\sqrt{2}a^2\delta + 6a^2\delta$$

$$y_G = \frac{5\sqrt{2}a^2\delta + 6a^2\delta}{2\sqrt{2}a\delta + 4a\delta} = \frac{a^2\delta(5\sqrt{2} + 6)}{a\delta(2\sqrt{2} + 4)} = 1,914a \quad G(0; 1,914a)$$

$$I_{x_G}^{(1)} = I_{x_{G1}} + A^{(1)}(y_G - y_{G1})^2 = \frac{1}{12} \delta l^3 \left(\frac{\sqrt{2}}{2}\right)^2 + (a\sqrt{2}\delta) \left(1,914a - \left(2a + \frac{a}{2}\right)\right)^2 = \frac{1}{12} \delta l^3 \frac{1}{2} + (a\sqrt{2}\delta) \cdot \left(1,914a - 2a - 0,5a\right)^2 = \frac{1}{24} \delta l^3 + (a\sqrt{2}\delta) \cdot \left(-0,586a\right)^2 = \frac{1}{24} \delta (a\sqrt{2})^3 + 0,602 a^3 \delta = 0,117 a^3 \delta + 0,602 a^3 \delta = 0,719 a^3 \delta$$

$$I_{x_G}^{(2)} = I_{x_{G2}} + A^{(2)}(y_G - y_{G2})^2 = 0 + (2a\delta) (1,914a - 2a)^2 = 0,0147 a^3 \delta$$

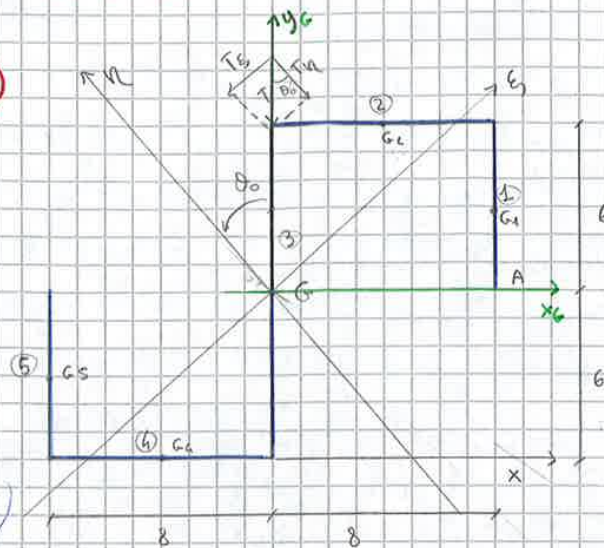
$$I_{x_G}^{(3)} = I_{x_{G3}} + A^{(3)}(y_G - y_{G3})^2 = \frac{\delta \cdot (2a)^3}{12} + (2a\delta) (1,914a - a)^2 = 0,67 a^3 \delta + 1,67 a^3 \delta = 2,34 a^3 \delta$$

$$I_{x_{TOT}} = 2 \cdot (0,602 a^3 \delta) + 0,0147 a^3 \delta + 2,34 a^3 \delta = 3,56 a^3 \delta$$

TEMA D'ESAME 22/9/1994

ES. 3)

S=1



$$A^{(1)} = 6 \cdot 1 = 6$$

$$A^{(2)} = 8 \cdot 8 = 8$$

$$A^{(3)} = 12$$

$$A^{(4)} = 8$$

$$A^{(5)} = 6$$

$$A_{tot} = 40$$

Sezione di simmetria : baricentro = centro geometrico

$$I_{xG}^{(1)} = I_{xG1} + A^{(1)}(y_G - y_{G1})^2 = \frac{1 \cdot 6^3}{12} + 6 \cdot (0 - 3)^2 = 72$$

$$I_{xG}^{(2)} = I_{xG2} + A^{(2)}(y_G - y_{G2})^2 = 0 + 8 \cdot (0 - 6)^2 = 288$$

$$I_{xG}^{(3)} = I_{xG3} + A^{(3)}(y_G - y_{G3})^2 = \frac{1 \cdot 12^3}{12} + 12(0 - 0)^2 = 144$$

$$I_{xG_{tot}} = 2 \cdot 72 + 2 \cdot 288 + 144 = 864$$

$$I_{yG}^{(1)} = I_{yG1} + A^{(1)}(x_G - x_{G1})^2 = 0 + 6 \cdot (0 - 8)^2 = 384$$

$$I_{yG}^{(2)} = I_{yG2} + A^{(2)}(x_G - x_{G2})^2 = \frac{1 \cdot 8^3}{12} + 8 \cdot (0 - 4)^2 = 170,67$$

$$I_{yG}^{(3)} = I_{yG3} + A^{(3)}(x_G - x_{G3})^2 = 0 + 12(0 - 0)^2 = 0$$

$$I_{yG_{tot}} = 2 \cdot 384 + 2 \cdot 170,67 = 1109,34$$

$$I_{xG yG}^{(1)} = I_{xG yG1} + A^{(1)}(y_G - y_{G1})(x_G - x_{G1}) = 0 + 6(0 - 3)(0 - 8) = 144$$

$$I_{xG yG}^{(2)} = I_{xG yG2} + A^{(2)}(y_G - y_{G2})(x_G - x_{G2}) = 0 + 8(0 - 6)(0 - 4) = 192$$

$$I_{xG yG}^{(3)} = I_{xG yG3} + A^{(3)}(y_G - y_{G3})(x_G - x_{G3}) = 0 + 12(0 - 0)(0 - 0) = 0$$

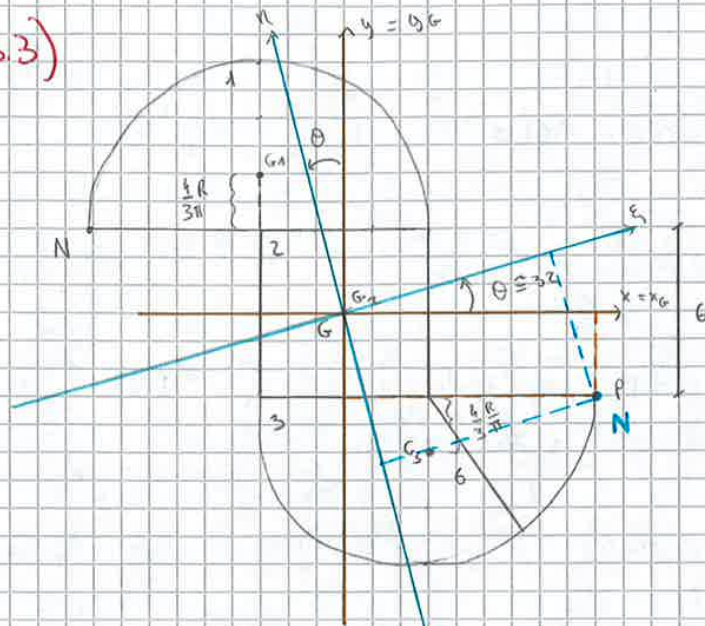
$$I_{xG yG_{tot}} = 2(144 + 192) = 336 \cdot 2 = 672$$

TEMA D'ESAME

19/9/2011

COMPITO I

es. 3)



$$G_1 = \left( -3, 3 + \frac{4}{3\pi} \cdot 6 \right)$$

$$= \left( -3, 3 + \frac{8}{\pi} \right)$$

$$G_2 = (0, 0)$$

$$G_3 = \left( 3, -\left( 3 + \frac{4}{3\pi} \cdot 6 \right) \right)$$

$$= \left( 3, -3 - \frac{8}{\pi} \right)$$

$$N = 10 \text{ kN}$$

$$A_1 = A_3 = \frac{\pi}{2} R^2 = \frac{\pi}{2} \cdot 6^2 = \frac{36\pi}{2} = 18\pi$$

$$A_2 = 6 \cdot 6 = 36$$

$$A_{\text{tot}} = 2 \cdot 18\pi + 36 = 36\pi + 36 = 36(\pi + 1)$$

$$S_y^{(1)} = y_{G1} \cdot A^{(1)} = \left( 3 + \frac{8}{\pi} \right) \cdot 18\pi = 313,65$$

$$S_y^{(2)} = y_{G2} \cdot A^{(2)} = 0$$

$$S_y^{(3)} = y_{G3} \cdot A^{(3)} = \left( -3 - \frac{8}{\pi} \right) \cdot 18\pi = -313,65$$

$$S_{y_{\text{tot}}} = 0 \quad y_G = 0$$

G baricentro (0, 0) → coincide con G2

$$S_{x_{\text{tot}}} = 0 \quad x_G = 0$$

$$I_{x_G^{(1)}} = I_{x_{G1}} + A(y_G - y_{G1})^2 = \left( \frac{\pi}{8} - \frac{8}{9\pi} \right) 6^4 + (18\pi) \cdot \left( 3 + \frac{8}{\pi} \right)^2$$

$$= 142,24 + 1739,63 = 1881,87$$

$$I_{x_G^{(3)}} = I_{x_G^{(1)}} = 1881,87$$

$$I_{x_G^{(2)}} = I_{x_{G2}} + A(y_G - y_{G2})^2 = \frac{1}{12} \cdot 6 \cdot 6^3 + 0 = 108$$

$$I_{x_G_{\text{tot}}} = 3871,74$$

$$\sigma_z = \frac{N}{A} + \frac{M_x}{I_x} \cdot y - \frac{M_y}{I_y} \cdot x \quad \rightarrow \quad \sigma_z = \frac{N}{A} + \frac{M_\xi}{I_\xi} \eta - \frac{M_\eta}{I_\eta} \xi$$

$$M_\xi = N \cdot e_\eta \quad M_\eta = -N \cdot e_\xi$$

$$P_{x_0 y_0} = \begin{pmatrix} x \\ y \end{pmatrix} = \begin{pmatrix} 9 \\ -3 \end{pmatrix} \quad P_{\xi \eta} = ?$$

$$\begin{bmatrix} 9 \\ -3 \end{bmatrix} = \begin{bmatrix} \cos \alpha & \sin \alpha \\ -\sin \alpha & \cos \alpha \end{bmatrix} \begin{bmatrix} \xi \\ \eta \end{bmatrix} \quad \begin{bmatrix} \xi \\ \eta \end{bmatrix} = \begin{bmatrix} \cos \alpha & \sin \alpha \\ -\sin \alpha & \cos \alpha \end{bmatrix} \begin{bmatrix} 9 \\ -3 \end{bmatrix}$$

$$\xi = -3 \cos \alpha + 9 \sin \alpha = -3 \cos 32,66 + 9 \sin 32,66 = 5,96$$

$$\eta = +3 \sin \alpha + 9 \cos \alpha = -9 \sin 32,66 + 3 \cos 32,66 = -7,38$$

$$P_{\xi \eta} = (5,96; -7,38)$$

$$\begin{aligned} \xi &= e_\xi \\ \eta &= e_\eta \end{aligned}$$

$$M_\xi = 10^4 \cdot -7,38 = -73,8 \cdot 10^3$$

$$M_\eta = -10^4 \cdot 5,96 = -59,6 \cdot 10^3$$

misura in cm  $\rightarrow$  mm  
sfuerzo in kN  $\rightarrow$  N

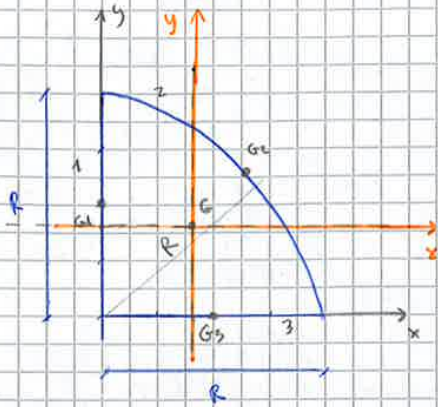
$$\sigma_z = \frac{10 \cdot 10^3}{26(11+1) \cdot 10^2} + \frac{-73,8 \cdot 10^3}{5078,47} \eta - \frac{(-59,6) \cdot 10^3}{937,01} \xi$$

$$= \dots \rightarrow m P(5,96; -7,38)$$

4

TEMA D'ESAME 10/5/1994

ES.3)



$$G_1 = \left(0; \frac{R}{2}\right)$$

$$G_3 = \left(\frac{R}{2}; 0\right)$$

$$G_2 = \left(\frac{2}{\pi}R; \frac{2}{\pi}R\right)$$

N.B. qualsiasi sistema di riferimento che passa per G è baricentrico ( $S_x = S_y = 0$ )

$$\left. \begin{aligned} A_1 &= RS \\ A_3 &= R \cdot S \\ A_2 &= \frac{\pi}{2}SR \end{aligned} \right\} A_{tot} = RS \left(z + \frac{\pi}{2}\right)$$

$$\frac{4 + \pi}{2}$$

$$G = (0,42R; 0,42R)$$

$$\left. \begin{aligned} S_x^{(1)} &= y_{G1} \cdot A^{(1)} = \frac{R}{2} \cdot RS = \frac{R^2 S}{2} \\ S_x^{(2)} &= y_{G2} \cdot A^{(2)} = \frac{2}{\pi} R \cdot \left(\frac{\pi}{2} SR\right) = SR^2 \\ S_x^{(3)} &= y_{G3} \cdot A^{(3)} = 0 \end{aligned} \right\}$$

$$S_{x,tot} = \frac{R^2 S}{2} + \frac{2}{2} SR^2 = \frac{3}{2} R^2 S$$

$$y_G = \frac{\frac{3}{2} R^2 S}{R \cdot \left(z + \frac{\pi}{2}\right)} = \frac{3}{2} \cdot \frac{2}{4 + \pi} R = \frac{3}{4 + \pi} R = 0,42R$$

$$\left. \begin{aligned} S_y^{(1)} &= x_{G1} \cdot A^{(1)} = 0 \\ S_y^{(2)} &= x_{G2} \cdot A^{(2)} = \frac{2}{\pi} R \cdot \left(\frac{\pi}{2} SR\right) = SR^2 \\ S_y^{(3)} &= x_{G3} \cdot A^{(3)} = \frac{R}{2} \cdot RS = \frac{R^2 S}{2} \end{aligned} \right\}$$

$$S_{y,tot} = \frac{3}{2} R^2 S$$

$$x_G = \frac{3}{4 + \pi} R = 0,42R$$

$$I_{x_G}^{(1)} = I_{x_{G1}}^{(1)} + A^{(1)} (y_G - y_{G1})^2 = \frac{S \cdot R^3}{12} + RS \left(0,42R - \frac{R}{2}\right)^2 = \frac{1}{12} SR^3 + 0,089 SR^3 = 0,089 SR^3$$



TRATTO BC:

← N =  $\frac{ql}{4}$

+↑ T =  $\frac{ql}{4} - qlz = q\left(\frac{l}{4} - z\right)$

T(0) = T<sub>B</sub> =  $\frac{ql}{4}$

T(l) = T<sub>C</sub> =  $q\left(\frac{l}{4} - l\right) = q\left(\frac{l}{4} - \frac{4l}{4}\right) = q\left(-\frac{3}{4}l\right) = -\frac{3}{4}ql$

↺ M =  $\frac{ql}{4}z + ql \cdot l - qlz \cdot \frac{z}{2}$   
 $= q\left(\frac{lz}{4} + \frac{l^2}{4} - \frac{z^2}{2}\right)$

M(0) = M<sub>B</sub> =  $\frac{ql^2}{4}$

M(l) = M<sub>C</sub> =  $q\left(\frac{l^2}{4} + \frac{l^2}{4} - \frac{l^2}{2}\right) = q\left(\frac{l^2 + l^2 - 2l^2}{4}\right) = 0$

altro punto parabola:

$\frac{dM}{dz} = 0 \quad T = 0 \quad q\left(\frac{l}{4} - z\right) = 0 \rightarrow z = \frac{l}{4}$

↪ M( $\frac{l}{4}$ ) =  $\frac{9}{32} ql^2$

TRATTO DC

← N = 0

+↑ T = -ql

↺ M =  $ql^2 - qlz = ql(l - z)$

M(0) = M<sub>D</sub> =  $ql^2$

M(l) = M<sub>C</sub> =  $ql^2 - ql^2 = 0$

TRATTO CE

← N =  $\frac{ql}{4} - ql = \frac{ql - 4ql}{4} = -\frac{3}{4}ql$

+↑ T =  $\frac{ql}{4} - ql = -\frac{3}{4}ql$

T =  $\frac{dM}{dz} \quad M = \int T dz$

↺ M =  $\frac{ql}{4}z + ql \cdot l - ql \cdot l - ql \cdot (z - \frac{l}{2}) - ql^2$   
 $= \frac{ql}{4}z + \frac{ql^2}{4} - ql^2 - qlz + \frac{ql^2}{2} - ql^2$   
 $= \frac{qlz}{4} + \frac{ql^2}{4} - 4ql^2 - 4qlz + \frac{2ql^2}{2} - 4ql^2 = \frac{5ql^2 - 3qlz}{4}$

M(l) = M<sub>C</sub> =  $\frac{5ql^2 - 3ql^2}{4} = \frac{2ql^2}{4} = \frac{ql^2}{2}$

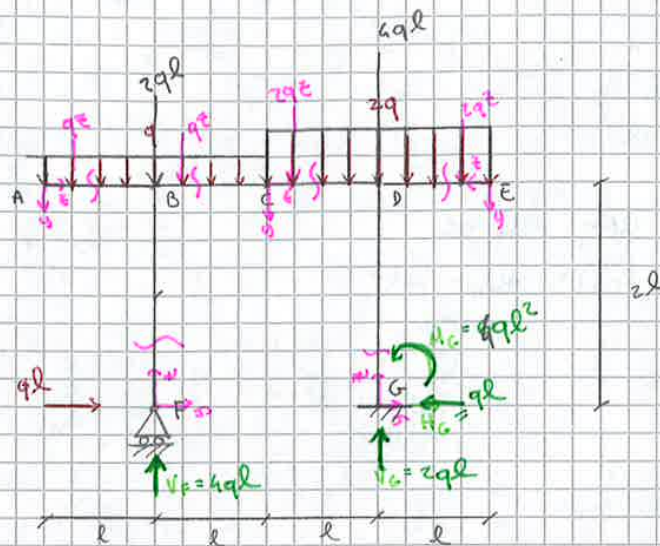
M(2l) = M<sub>E</sub> =  $\frac{5ql^2 - 6ql^2}{4} = -\frac{ql^2}{4} = -\frac{ql^2}{4}$

M =  $-\frac{3}{4}qlz$

M(0) = M<sub>C</sub> = 0

M(l) = M<sub>E</sub> =  $-\frac{3}{4}$

TEMA D'ESAME 8 settembre 1996 ESERCIZIO 1



4 incognite  
 $\Downarrow$   
 4 equazioni

REAZIONI VINCOLARI

$$\rightarrow \quad ql + H_G = 0 \quad \rightarrow \quad H_G = -ql$$

$$+\uparrow \quad V_F - 2ql - 4ql + V_G = 0 \quad \rightarrow \quad V_F + V_G - 6ql = 0$$

$$\begin{aligned} \odot \quad M(F) &= -4ql \cdot 2l + M_G + \cancel{H_G \cdot 2l} + V_G \cdot 2l \\ &= -8ql^2 + M_G - \cancel{2ql^2} + V_G \cdot 2l \\ &= -8ql^2 + M_G + V_G \cdot 2l \end{aligned}$$

eq. ausiliarie

$$\begin{aligned} \odot \quad M(C) &= -V_F \cdot l + 2ql \cdot l + ql \cdot 2l = 0 \\ \text{da sx} \quad &= -V_F \cdot l + 2ql^2 + 2ql^2 = 0 \\ &= -V_F \cdot l + 4ql^2 = 0 \quad \rightarrow \quad V_F = \frac{4ql^2}{l} = 4ql \end{aligned}$$

$$4ql + V_G - 6ql = 0 \quad \rightarrow \quad V_G = 2ql$$

$$-8ql^2 + M_G + 2ql \cdot 2l = 0 \Rightarrow -8ql^2 + M_G + 4ql^2 = 0$$

$$\quad \quad \quad M_G = 4ql^2$$

TRATTO AB

$\leftarrow^+$   $N = 0$

$\uparrow$   $T = qz$

$T(0) = T_A = 0$

$T(l) = T_B = ql$

$\curvearrowright$   $M = -qz \cdot \frac{z}{2} = -\frac{qz^2}{2}$

$M(0) = M_A = 0$

$M(l) = M_B = -\frac{ql^2}{2}$

TRATTO BF

$\leftarrow^+$   $N = -4ql$

$\uparrow$   $T = -ql$

$\curvearrowright$   $M = -ql \cdot z$

$M(0) = M_F = 0$

$M(2l) = M_B = -ql \cdot 2l = -2ql^2$

TRATTO BC

$\leftarrow^+$   $N = -ql$

$\uparrow$   $T = -qz + 4ql$

$T(l) = T_B = -ql + 4ql = 3ql$

$T(2l) = T_C = -q \cdot 2l + 4ql = 2ql$

$\curvearrowright$   $M = 4ql \cdot (z-l) - ql \cdot 2z - qz \cdot \frac{z}{2}$

$= 4qlz - 4ql^2 - 2ql^2 - \frac{qz^2}{2}$

$= 4qlz - 6ql^2 - \frac{qz^2}{2}$

$M(0) = 4ql^2 - 6ql^2 - \frac{ql^2}{2} = \frac{8ql^2 - 12ql^2 - ql^2}{2} = -\frac{5}{2}ql^2$

$M(2l) = 8ql^2 - 6ql^2 - \frac{q(4l)^2}{2} = (8-6-2)ql^2 = 0$

TRATTO CD

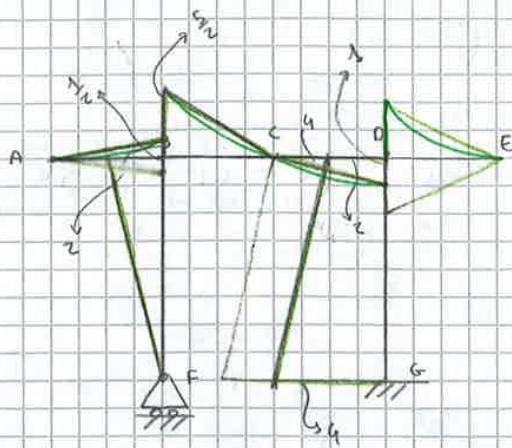
$\leftarrow^+$   $N = -ql$

$\uparrow$   $T = 4ql - 2ql - 2qz = 2ql - 2qz$

$T(0) = T_C = 2ql$

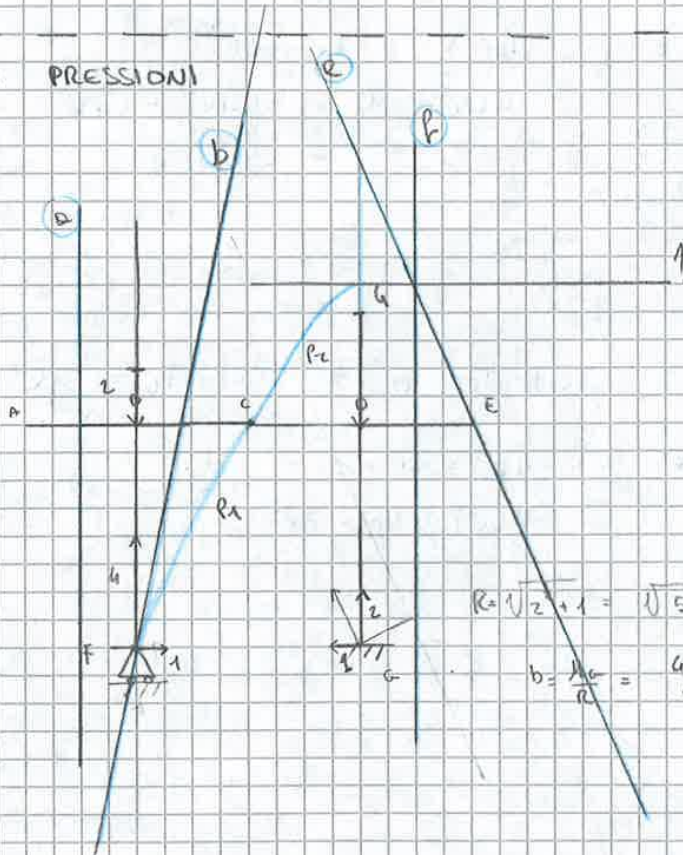
$T(l) = T_D = 0$

$\curvearrowright$   $M = 4ql \cdot (l+z) - 2ql \cdot (l+z) - ql \cdot 2l - 2qz \cdot \frac{z}{2}$



$$\frac{M}{ql^2}$$

CORVA DELLE PRESSIONI

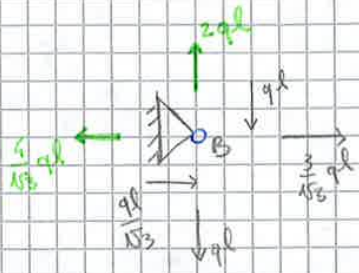


$$R = \sqrt{z^2 + 1} = \sqrt{5} \, ql$$

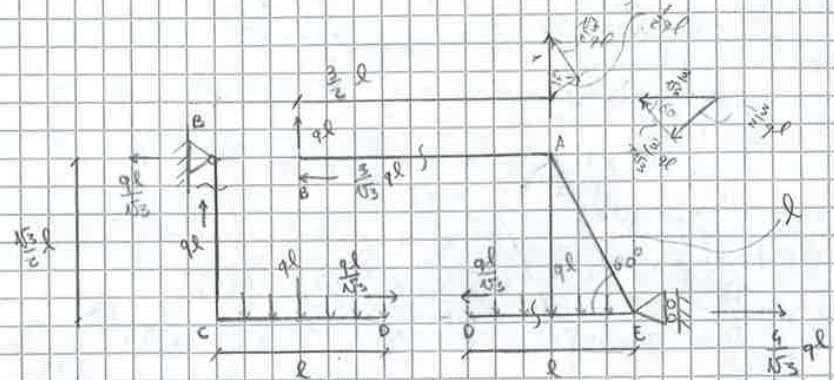
$$b = \frac{M_0}{ql} = \frac{ql^2}{\sqrt{5}ql} = \frac{q}{\sqrt{5}} l$$

$$\frac{1}{2}ql^2 - H_0 \frac{\sqrt{3}}{2}l = 0 \quad \rightarrow \quad H_0 = \frac{\frac{1}{2}ql^2}{\frac{\sqrt{3}}{2}l} \quad + \quad H_0 = \frac{1}{2}ql^2 \cdot \frac{2}{\sqrt{3}l} = \frac{ql}{\sqrt{3}}$$

Verifica nodo B:



reazioni che i tratti 1 e 2 scaricano su cerniera B



SOLLECITAZIONI:

• MOMENTO M

TRATTO BA

$$\begin{aligned} \curvearrowright M &= ql \cdot z & M(0) &= M_B = 0 \\ M\left(\frac{3}{2}l\right) &= M_A = ql \cdot \left(\frac{3}{2}l\right) = \frac{3}{2}ql^2 \end{aligned}$$

TRATTO AE

$$\begin{aligned} \curvearrowright M &= \frac{ql}{2} \cdot z - \frac{3}{2}ql \cdot z & M(0) &= M_A = 0 \\ M(l) &= M_E = \frac{ql^2}{2} - \frac{3}{2}ql^2 = -\frac{2}{2}ql^2 = -ql^2 \end{aligned}$$

TRATTO DE

$$\begin{aligned} \curvearrowright M &= ql \cdot \frac{z}{2} & M(0) &= M_D = 0 \\ M(x) &= M_E = ql \cdot \frac{x}{2} \end{aligned}$$

TRATTO BC

$$\begin{aligned} \curvearrowright M &= -\frac{ql}{\sqrt{3}} \cdot z & M(0) &= M_B = 0 \\ M\left(\frac{\sqrt{3}}{2}l\right) &= M_C = -\frac{ql}{\sqrt{3}} \cdot \frac{\sqrt{3}l}{2} = -\frac{ql^2}{2} \end{aligned}$$

• TAGLIO T

TRATTO BA

$$+\uparrow T = ql$$

TRATTO DE

$$+\uparrow T = -qz$$

$$\begin{aligned} T(0) &= 0 = T_D \\ T(x) &= T_E = -ql \end{aligned}$$

TRATTO BC

$$+\uparrow T = -\frac{ql}{\sqrt{3}}$$

• SFORZO N

TRATTO AE

$$+\uparrow T = \frac{1}{2}ql - \frac{3}{2}ql = -ql$$

TRATTO BA

$$\leftarrow N = \frac{3}{\sqrt{3}}ql$$

TRATTO DE

$$\leftarrow N = \frac{ql}{\sqrt{3}}$$

TRATTO BC

$$\leftarrow N = ql$$

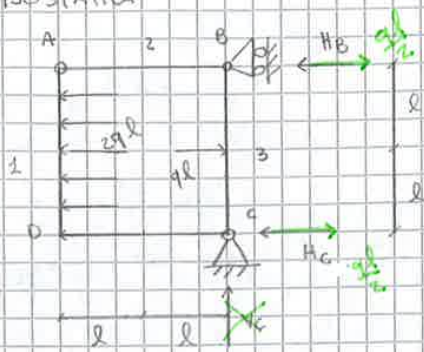
TRATTO AE

$$\leftarrow N = \frac{\sqrt{3}}{2}ql + \frac{3}{2\sqrt{3}}ql = \frac{3}{\sqrt{3}}ql$$

TEMA D'ESAME

12/6/2007

ES. 1) ISOSTATICA



3 corpi :

$3 \cdot 3 = 9$

$(2 \times 3) + (2 + 2) = 9$   
interni esterni

➤ REAZIONI VINCOLI:

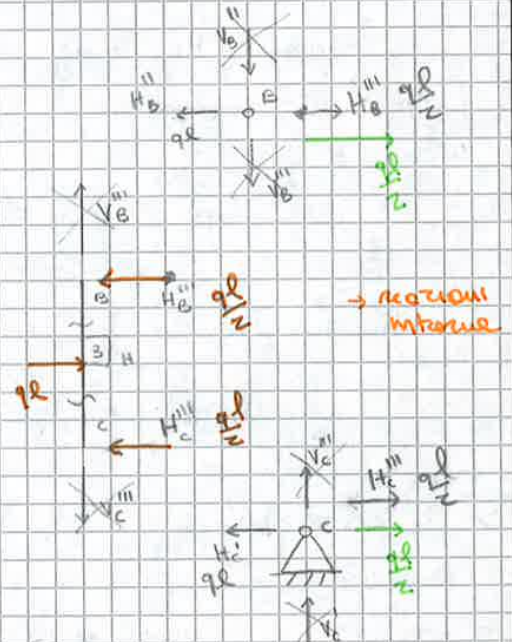
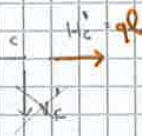
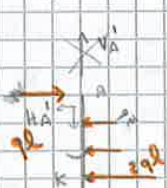
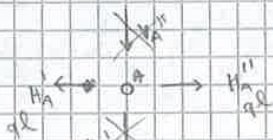
sezioni esterne

$\rightarrow -H_c - H_B + ql - 2ql = 0 \rightarrow -H_c + \frac{ql}{2} + ql - 2ql = 0 \rightarrow H_c = -\frac{ql}{2}$

$\uparrow V_c = 0$

$\curvearrowright M(c) = -ql \cdot l + H_B \cdot 2l + 2ql \cdot l = 0$

$H_B = \frac{-ql^2}{2l} = -\frac{ql}{2}$



sezioni interne

CORPO 1:

$\rightarrow -H_A - 2ql + H_c = 0 \rightarrow H_c = H_A + 2ql \rightarrow H_c = -ql + 2ql = ql$

$\uparrow V_A - V_c = 0 \rightarrow V_A = V_c \rightarrow V_c = 0$

$\curvearrowright M(A) = -2ql \cdot l - V_c \cdot 2l + H_c \cdot 2l = 0$

$\curvearrowright M(c) = 2ql \cdot l + H_A \cdot 2l - V_A \cdot 2l = 0 \rightarrow H_A = \frac{V_A \cdot 2l - 2ql^2}{2l} = \frac{2l(V_A - ql)}{2l}$

$-2ql^2 - V_A \cdot 2l + H_A \cdot 2l + 4ql^2 = 0$

$-2ql^2 - V_A \cdot 2l + (V_A - ql) \cdot 2l + 4ql^2 = 0$

$-2ql^2 - V_A \cdot 2l + V_A \cdot 2l - 2ql^2 + 4ql^2 = 0$

$H_A = \frac{-2ql^2}{2l} = -ql$

$V_A = 0$

(da equazione corpo 2)

• TAGLIO T

TRATTO AB

$\uparrow T = 0$

TRATTO BH

$\uparrow T = -\frac{qz}{z}$

TRATTO HC

$\uparrow T = -\frac{ql}{z} + ql = \frac{-ql + zql}{z} = \frac{ql}{z}$

TRATTO CD

$\uparrow T = 0$

TRATTO AD

$\uparrow T = ql - qz$

$T(d) = T_A = ql$

$T(l) = T_C = 0$

$T(l) = T_D = -ql$

• SFORZO N

TRATTO AB

$\pm N = ql$

TRATTO BC

$\pm N = 0$

TRATTO CD

$\pm N = ql$

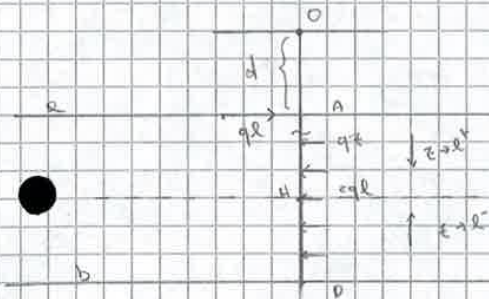
TRATTO AD

$\pm N = 0$

➤ CURVA DELLE PRESSIONI (USO REAZIONI INTERNE):

TRATTO AD

ci sono solo forze orizzontali, no forze verticali → non abbiamo → una parabola, ma il cdp degenera



$\sum M(z) = ql \cdot d - qz \left( d + \frac{z}{2} \right) = 0$

$ql \cdot d - qz \cdot d - \frac{qz^2}{2} = 0$

$d(l - z) - \frac{z^2}{2} = 0$

$d = \frac{z^2}{2(l - z)}$

→ distanza a cui applicata la risultante delle forze

per  $z < l$   
 $N > 0$   
 $D > 0$   
 $d(z) > 0$  → retta usc di A (sopra A)

per  $z > l$   
 $N < 0$   
 $D < 0$   
 $d(z) < 0$  → retta usc di A (sotto A)

$z \rightarrow l^+$   $d = +\infty$  fascio di rette da A verso +∞

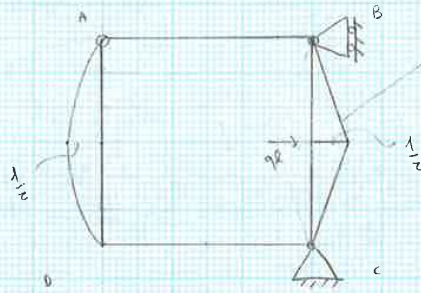
$z \rightarrow l^-$   $d = -\infty$  fascio di rette da D verso -∞

$d = \frac{(l^+)^2}{2(l - (l^+))}$   
 un pol' piccolo di l  
 $d = \frac{(l^+)^2}{0^+} = +\infty$

$d = \frac{(l^-)^2}{2(l - (l^-))}$   
 un pol' grande di l  
 $d = \frac{(l^-)^2}{0^-} = -\infty$

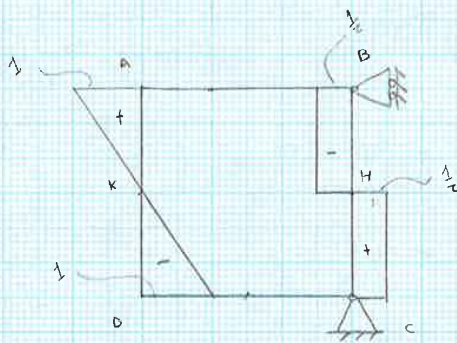
ES. 1 ISOSTATICA

1

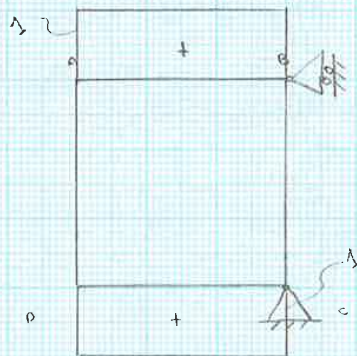


discontinuità di tipo cuspidale equivalente alla presenza della forza applicata

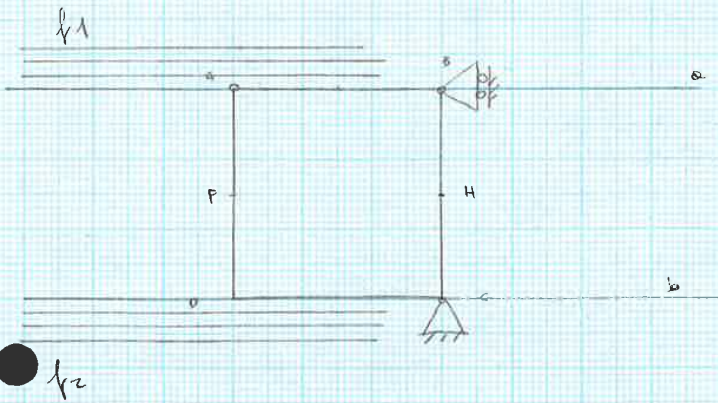
$$\frac{M}{ql^2}$$



$$\frac{T}{ql}$$



$$\frac{N}{ql}$$



TRATTO	cdp
AB	retta a
BH	retta a
HC	retta b
AF	$f_1$
FD	$f_2$





TRATTO BE

$$M = \frac{5}{8} ql \cdot z$$

TRATTO EC

$$M = -\frac{5}{4} ql \cdot \frac{2\sqrt{z}}{2} + \frac{5}{8} ql \cdot \left( l + \frac{2\sqrt{z}}{2} \right)$$

$$M(c) = M_E = \frac{5}{8} ql^2$$

$$M(l\sqrt{z}) = M_C = 0$$

• TAGLIO T ↑

TRATTO AD

$$T = \frac{3}{8} ql - qlz$$

$$T(b) = T_A = \frac{3}{8} ql$$

$$T(l) = T_b = \frac{3}{8} ql - ql = \frac{(3-8)}{8} ql = -\frac{5}{8} ql$$

TRATTO DC

$$T = \frac{3\sqrt{z}}{16} ql + \frac{3\sqrt{z}}{8} ql - \frac{5\sqrt{z}}{2} ql = \frac{\sqrt{z}}{16} ql$$

TRATTO BE

$$T = \frac{5}{8} ql$$

TRATTO EC

$$T = -\frac{5\sqrt{z}}{4} ql + \frac{5\sqrt{z}}{8} ql = -\frac{5\sqrt{z}}{16} ql$$

• SFORZO N ←

TRATTO AD

$$N = -\frac{3}{4} ql$$

TRATTO DC

$$N = \frac{3\sqrt{z}}{16} ql - \frac{\sqrt{z}}{2} ql - \frac{3\sqrt{z}}{8} ql = -\frac{11\sqrt{z}}{16} ql$$

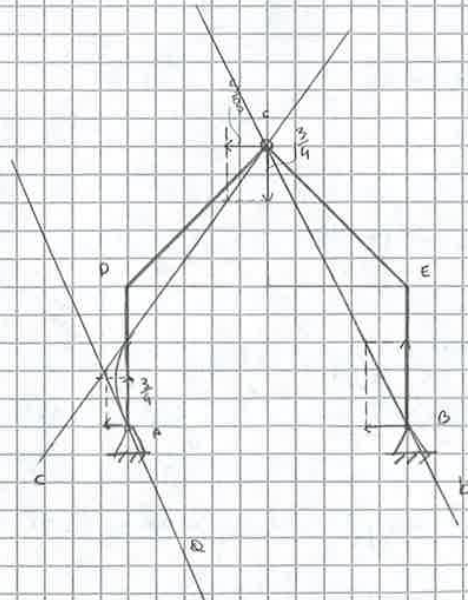
TRATTO BE

$$N = -\frac{5}{4} ql$$

TRATTO EC

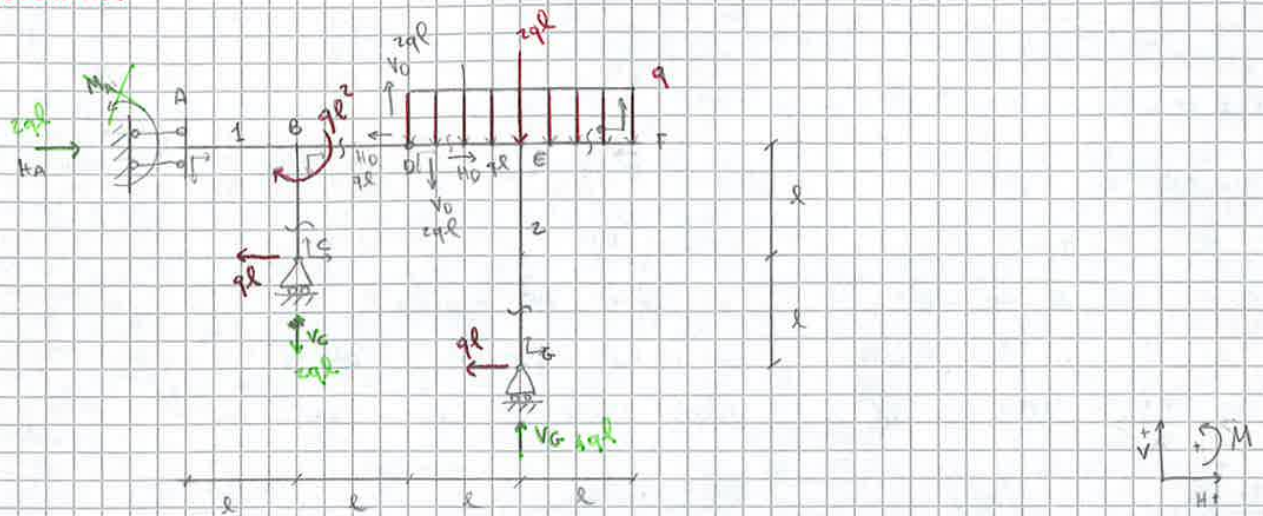
$$N = -\frac{5\sqrt{z}}{8} ql - \frac{5\sqrt{z}}{4} ql = -\frac{15\sqrt{z}}{16} ql$$

tratto	cdp
AD	parabola p
DC	retta c
CEB	retta b



TEMA D'ESAME 30/6/2008

ES. 1 )  
ISOSTATICA



PUNTO 1)  $M, N, T$  e curva delle pressioni

REAZIONI VINCOLARI :

$$\rightarrow H_A - ql - ql = 0 \rightarrow H_A = 2ql$$

$$\uparrow V_c + V_g - 2ql = 0 \rightarrow V_g = 2ql + 2ql = 4ql$$

$$\curvearrowright M(G) = -ql^2 + ql \cdot l - V_c \cdot 2l - H_A \cdot 2l + M_A = 0$$

curva 1:

$$\curvearrowright M(0) = M_A - ql^2 - ql \cdot l - V_c \cdot l = 0$$

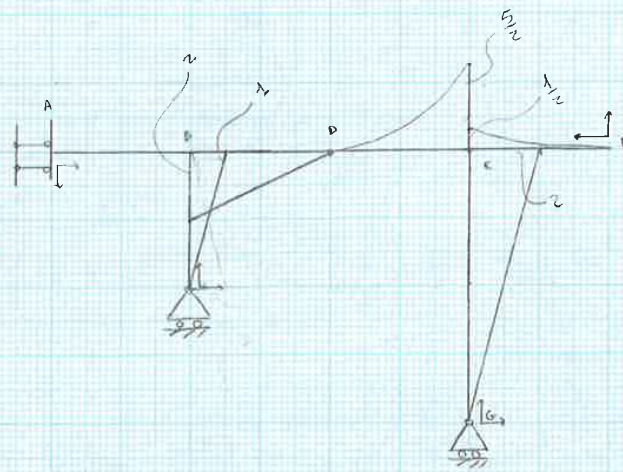
$$M_A = V_c l + ql^2 + ql^2 = V_c l + 2ql^2 \rightarrow M_A = -2ql^2 + 2ql^2 = 0$$

$$-ql^2 + ql^2 - V_c \cdot 2l - (2ql) \cdot (2l) + (V_c l + 2ql^2) = 0$$

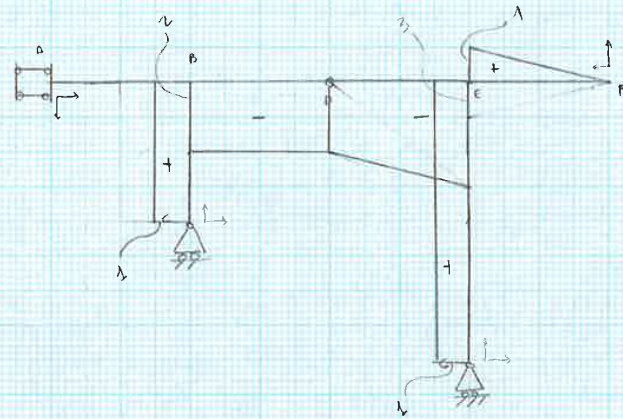
$$\cancel{-ql^2} - V_c \cdot 2l - 4ql^2 + V_c l + 2ql^2 = 0$$

$$-2ql^2 - V_c l = 0 \rightarrow V_c = \frac{-2ql^2}{l} = -2ql$$

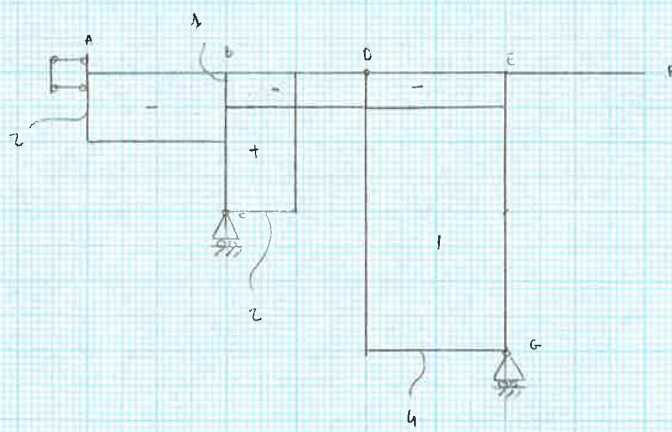
sist. di riferimento  
 fibre di sotto  
 (M+)



$$\frac{M}{ql^2}$$



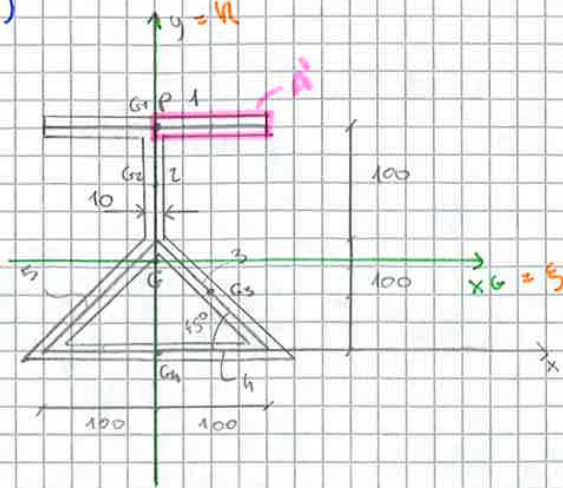
$$\frac{T}{ql}$$



$$\frac{N}{ql}$$



Punto 2)



$$A^{(1)} = 200 \cdot 10 = 2000$$

$$A^{(2)} = 100 \cdot 10 = 1000$$

$$A^{(3)} = 100\sqrt{2} \cdot 10 = 1414,21$$

$$A^{(4)} = 200 \cdot 10 = 2000$$

$$A_{tot} = A^{(1)} + A^{(2)} + 2A^{(3)} + A^{(4)} = 7828,42$$

$$\begin{aligned} S_x^{(1)} &= y_{G1} \cdot A^{(1)} = 200 \cdot 2000 = 400000 \\ S_x^{(2)} &= y_{G2} \cdot A^{(2)} = 150 \cdot 1000 = 150000 \\ S_x^{(3)} &= y_{G3} \cdot A^{(3)} = 50 \cdot 1414,21 = 70710,5 \\ S_x^{(4)} &= y_{G4} \cdot A^{(4)} = 0 \end{aligned}$$

$$S_{tot} = 620710,5 \quad 691421$$

$$y_G = \frac{S_{tot}}{A_{tot}} = \frac{620710,5}{7828,42} = 79,29 \quad 88,32$$

$$G = (0; 88,33)$$

$$I_{xG}^{(1)} = I_{xG1} + A^{(1)}(y_G - y_{G1})^2 = 0 + 2000 \left( \frac{88,33}{200} - 200 \right)^2 = 24940377,8$$

$$I_{xG}^{(2)} = I_{xG2} + A^{(2)}(y_G - y_{G2})^2 = \frac{10 \cdot 100^3}{12} + 1000 \left( \frac{88,33}{100} - 150 \right)^2 = 8833238,9$$

$$I_{xG}^{(3)} = I_{xG3} + A^{(3)}(y_G - y_{G3})^2 = \frac{10 \cdot (100\sqrt{2})^3 \cdot \sin^2 45^\circ}{12} + 1414,21 \cdot \left( \frac{88,33}{100\sqrt{2}} - 50 \right)^2 = 325628,9$$

$$I_{xG}^{(4)} = I_{xG4} + A^{(4)}(y_G - y_{G4})^2 = 0 + 2000 \left( \frac{88,33}{200} - 0 \right)^2 = 15604377,8$$

$$I_{xG_{tot}} = I_{xG}^{(1)} + I_{xG}^{(2)} + 2I_{xG}^{(3)} + I_{xG}^{(4)} = 51693783,63 \quad \text{mm}^4$$

$$I_{yG}^{(1)} = I_{yG1} + A^{(1)}(x_G - x_{G1})^2 = \frac{10 \cdot 200^3}{12} + 2000 \cdot (0 - 0)^2 = 6666666,6$$

$$I_{yG}^{(2)} = I_{yG2} + A^{(2)}(x_G - x_{G2})^2 = 0$$

$$I_{yG}^{(3)} = I_{yG3} + A^{(3)}(x_G - x_{G3})^2 = \frac{10 \cdot (100\sqrt{2})^3 \cos^2 45^\circ}{12} + 1414,21 \cdot (0 - 50)^2 = 4714036,3$$

$$I_{yG}^{(4)} = I_{yG4} + A^{(4)}(x_G - x_{G4})^2 = \frac{10 \cdot 200^3}{12} = 6666666,6$$

Von Mises :  $\sigma_{eq} = \sqrt{\sigma_e^2 + 3\tau_e^2} = \sqrt{293,44^2 + 3 \cdot (13,16)^2} = 294,32 > \sigma_{amm}$

sezione  
non verificata

$\overline{DE} \quad M = -qz \cdot \frac{z}{2}$

$\overline{FE} \quad M = qz \cdot \frac{z}{2}$

$M(0) = M_D = 0$

$M(0) = M_F = 0$

$M(l) = M_E = -\frac{ql^2}{2}$

$M(l) = M_E = \frac{ql^2}{2}$

①  $\overline{AC} \quad T = -\frac{ql}{2}$

$\overline{CD} \quad T = ql - qz$   
 $T(0) = T_C = ql$   
 $T(l) = T_D = 0$

$\overline{FE} \quad T = \frac{ql}{2}$

$\overline{DE} \quad T = -qz$   
 $T(0) = T_D = 0$   
 $T(l) = -ql$

②  $\overline{AC} \quad N = -ql$

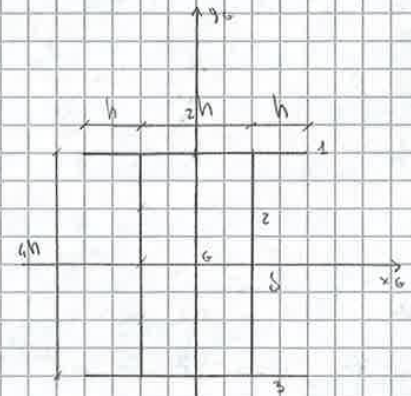
$\overline{DE} \quad N = -\frac{ql}{2}$

$\overline{AF} \quad N = \frac{ql}{2}$

$\overline{CD} \quad N = -\frac{ql}{2}$

$\overline{EB} \quad N = ql$

2)  $T_{max} = T_C = T_E = ql$



sezione chiusa simmetrica  $\Rightarrow \bar{x}_G = \frac{T_y \cdot S_x^{(n)}}{I_x}$

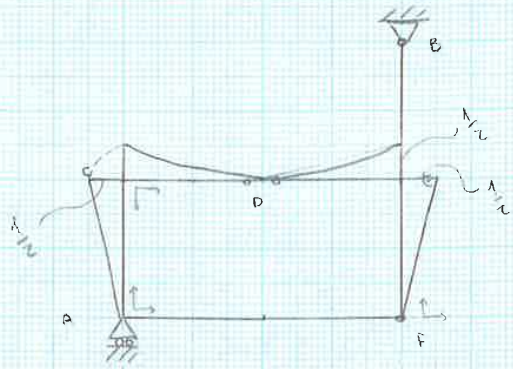
$A_1 = 4h \cdot \delta$

$A_2 = 4h \cdot \delta$

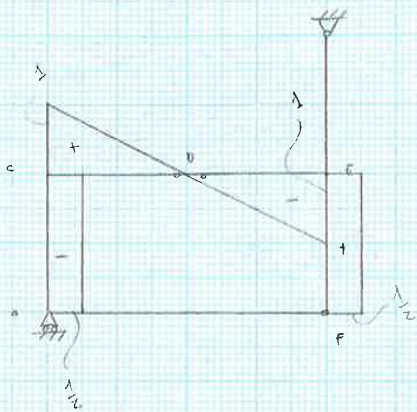
$A_3 = 4h \cdot \delta$

$$\begin{cases} I_{x_G}^{(1)} = I_{x_{G1}} + A^{(1)}(y_G - y_{G1})^2 = 0 + 4h\delta(0 - zh)^2 = 4h\delta \cdot (4h^2) = 16h^3\delta \\ I_{x_G}^{(2)} = I_{x_{G2}} + A^{(2)}(y_G - y_{G2})^2 = \frac{\delta \cdot (4h)^3}{12} + 4h\delta \cdot 0 = \frac{64\delta h^3}{12} \\ I_{x_G}^{(3)} = I_{x_{G3}} + A^{(3)}(y_G - y_{G3})^2 = 0 + 4h\delta(zh)^2 = 16h^3\delta \end{cases}$$

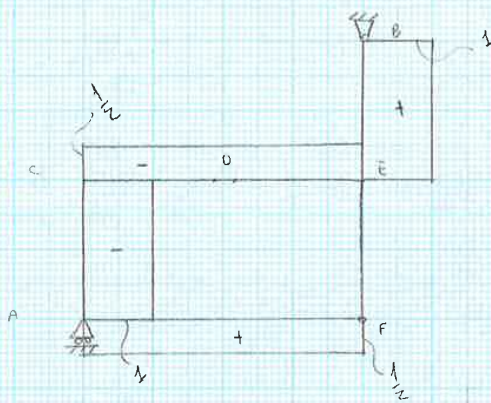
$$\begin{aligned} I_{x_G \text{ tot}} &= I_{x_G}^{(1)} + 2 I_{x_G}^{(2)} + I_{x_G}^{(3)} = 16h^3\delta + 2 \cdot \frac{64\delta h^3}{12} + 16h^3\delta \\ &= 32h^3\delta + \frac{128\delta h^3}{12} = \frac{384 + 128}{12} h^3\delta = \frac{512}{12} h^3\delta \\ &= \frac{128}{3} h^3\delta \end{aligned}$$



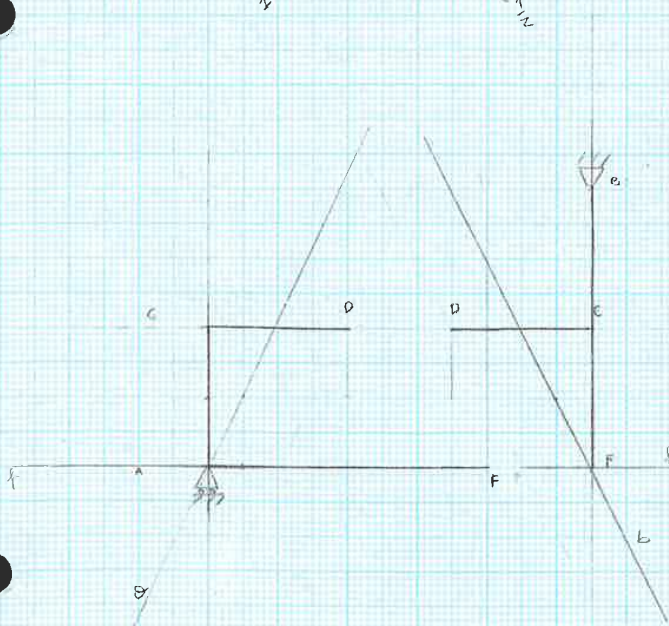
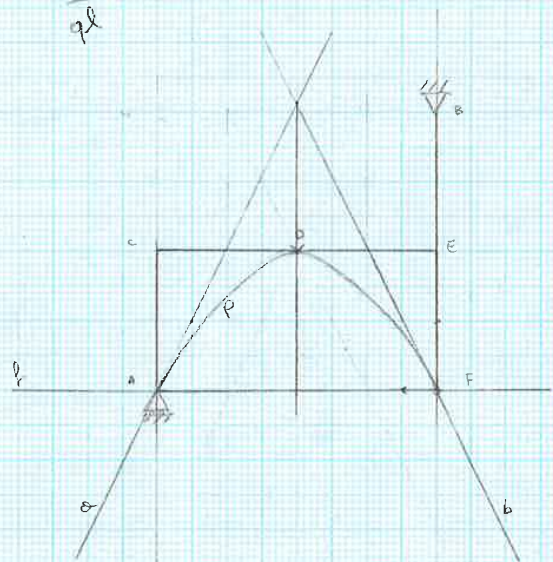
$$\frac{M}{qL^2}$$



$$\frac{T}{qL}$$



$$\frac{N}{qL}$$

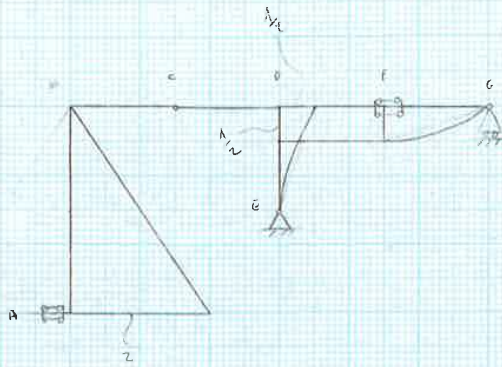


tratto	cdp
FA	retta f
Ac	retta a
FE	retta f
DE	retta b
CDE	parabola p

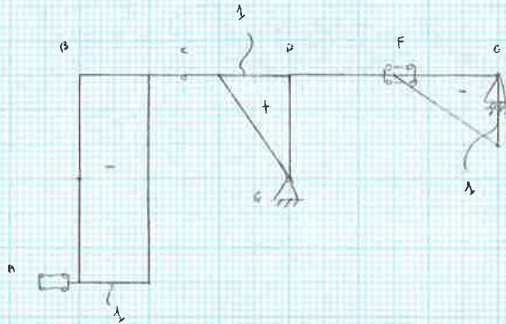
risultante forze da F

risultante forze da F

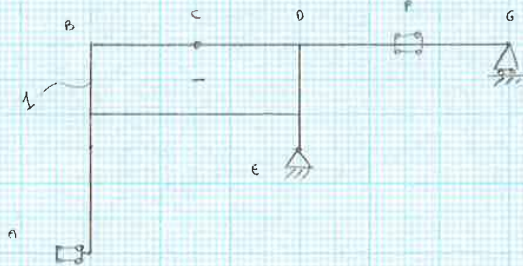




$$\frac{M}{ql}$$

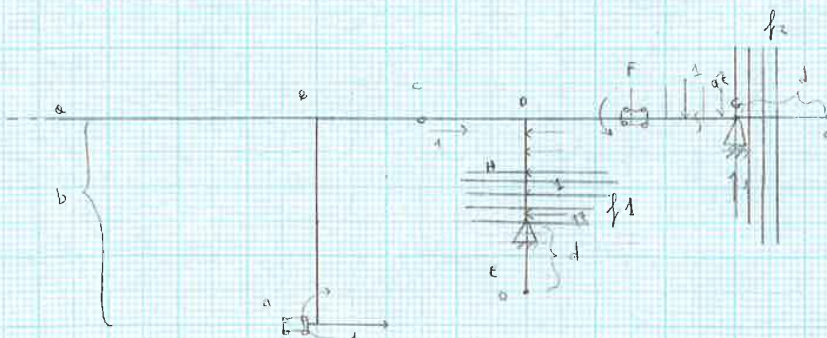


$$\frac{T}{ql}$$



$$\frac{N}{ql}$$

1,2



N.B. tratto FG:

$$M(x) = -ql \cdot d + qz \cdot \left(\frac{z}{2} + d\right)$$

$$-ld + \frac{z^2}{2} + zd = 0$$

$$d(-l+z) + \frac{z^2}{2} = 0$$

$$d = \frac{-\frac{z^2}{2}}{(-l+z)} = \frac{\frac{z^2}{2}}{(l-z)}$$

$$0 < z < l \rightarrow \begin{cases} z=0 & d=0 \\ z=l & d=+\infty \end{cases}$$

fz tra G e l'inf dx di G

$$a \cdot b = \frac{M}{K} = \frac{2ql^2}{12l} = 2l$$

N.B. tratto DE:

$$M(x) = qz \cdot \left(\frac{z}{2} + d\right)$$

$$q\frac{z^2}{2} + qzd = 0$$

$$\frac{z^2}{2} + zd = 0$$

$$d = \frac{-\frac{z^2}{2}}{z} = -\frac{z}{2}$$

$$0 < z < l \rightarrow \begin{cases} z=0 & d=0 \\ z=l & d=-\frac{l}{2} \end{cases}$$

f1 tra e e H

tratto	cdp
AD	retta a
DF	retta impropria all'∞
DE	fascio f1
FG	fascio fz





(T)

$\overline{AB}$   $T = 2ql$

$\overline{DE}$   $T = -ql$

$\overline{CD}$   $T = 2ql - 2ql = 0$

$T(0) = T_D = 0$   
 $T(l) = T_C = -ql$

$T(0) = T_C = 2ql$   
 $T(l) = T_D = 0$

$\overline{FG}$   $T = -ql$

$\overline{GH}$   $T = -ql - \frac{3}{2}ql$   
 $= -\frac{5}{2}ql$

(N)

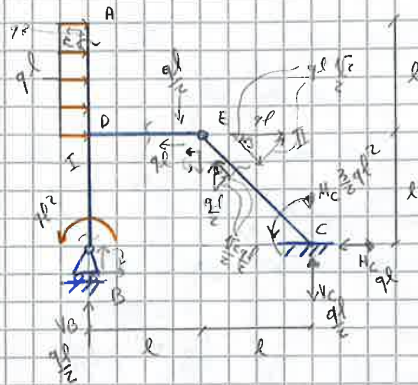
$\overline{CB}$   $N = +2ql$

$\overline{EF}$   $N = ql$

$\overline{FG}$   
 $\overline{GH}$   $N = -ql$

TEMA D'ESAME 3/7/2007 COMPITO II

ES.1)



reazioni vincolari

$$\rightarrow ql + H_c = 0 \rightarrow H_c = -ql$$

$$\uparrow V_B + V_c = 0$$

$$\hookrightarrow M(c) = -V_B \cdot 2l + ql^2 - ql \left( l + \frac{l}{2} \right) - M_c = 0$$

corpo II

$$\hookrightarrow M(E) = +V_c \cdot l + H_c \cdot l - M_c = 0$$

$$V_c \cdot l - ql^2 - M_c = 0 \rightarrow M_c = V_c \cdot l - ql^2 \quad \begin{aligned} M_c &= -\frac{ql^2}{2} - \frac{ql^2}{2} \\ &= -\frac{3}{2}ql^2 \end{aligned}$$

$$\begin{cases} V_B + V_c = 0 \rightarrow V_B = -V_c \\ -V_B \cdot 2l + ql^2 - \frac{3}{2}ql^2 - V_c \cdot l + ql^2 = 0 \end{cases} \quad V_B = \frac{ql}{2}$$

$$V_c \cdot 2l - V_c \cdot l + 2ql^2 - \frac{3}{2}ql^2 = 0$$

$$V_c \cdot l + \frac{ql^2}{2} = 0 \rightarrow V_c = -\frac{ql^2}{2l} = -\frac{ql}{2}$$

interne : corpo I

$$\rightarrow ql - H_c = 0 \rightarrow H_c = ql$$

$$\uparrow \frac{ql}{2} - V_c = 0 \rightarrow V_c = \frac{ql}{2}$$

SCELTAZIONI

$$\textcircled{M} \quad \overline{BD} \quad M = -ql^2$$

$$\overline{AD} \quad M = qz \cdot \frac{z}{2}$$

$$M(c) = M_D = 0$$

$$M(l) = M_D = \frac{ql^2}{2}$$

$$\overline{DE} \quad M = -\frac{ql}{2} \cdot z$$

$$M_E = M(c) = -\frac{ql}{2} \cdot 0 = 0$$

$$M_D = M(c) = -\frac{ql^2}{2}$$

$$\overline{EC} \quad M = ql \frac{\sqrt{2}}{2} \cdot z + \frac{ql}{2} \frac{\sqrt{2}}{2} \cdot z$$

$$M(c) = M_E = 0$$

$$M(2l\sqrt{2}) = M_c = ql \frac{\sqrt{2}}{2} \cdot (l\sqrt{2}) + \frac{ql}{2} \frac{\sqrt{2}}{2} \cdot (l\sqrt{2})$$

$$= ql^2 + \frac{ql^2}{2} = \frac{3}{2}ql^2$$